

FILE COPY

STORMWATER MANAGEMENT REPORT

PARKERS PLACE MULTI-FAMILY DEVELOPMENT PARK PLACE (MAP 11.1, LOT 11) EAST LYME, CT

PREPARED FOR

OWNER / APPLICANT PARKERS PLACE LLC PO BOX 817 EAST LYME, CT 06333

DATE:

SEPTEMBER 29, 2025

REVISED:

Received

OCT 9 2025

Town of East Lyme Land Use



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APPLICANT / SITE INFORMATION

OWNER / APPLICANT Parkers Place LLC PO Box 817 East Lyme, CT 06333 SITE

Map 11.1, Lot 11 Park Place

East Lyme, CT 06357

PROJECT DESCRIPTION AND PURPOSE

Parkers Place LLC is proposing to construct a multi-family development with associated amenities on a 6.98-acre parcel of land located on Park Place in East Lyme, CT. The subject parcel is identified as Map 11.1, Lot 11 on the Town of East Lyme Tax Assessor Mapping and is depicted on a map entitled "Topographic Survey Prepared for Pazz Construction LLC, Park Place - East Lyme, Connecticut", Date: January 23, 2023 as revised through 1-31-23, Scale: 1" = 50', prepared by Robert C. Simoni, Licensed Land Surveyor. The above-described parcel is hereinafter referred to as "Site".

The multi-family development will consist of the construction of 10 townhouse style buildings with a total of 60 residential two-bedroom units. Main access will be provided from the southeast via a

The full development will include the following improvements:

- 60 two-bedroom townhouse units in ten residential buildings
- 24' wide primary and secondary access driveways
- Pedestrian sidewalks with connection to Park Place
- 146 parking spaces including garages, driveways, and guest parking
- Pole-mounted area lighting of driveways and parking areas
- Exterior active and passive recreation areas and trails
- Stormwater management system consisting of collection, treatment, retention, and attenuation of peak flow rates to maintain existing drainage patterns and discharge conditions
- Sanitary sewer utility including extension of the existing public main in Park Place to serve the site and a private sanitary main to serve the development
- Private water main to serve the development with connection to the existing water main in
- Electric and telecommunication utility connections to the overhead utilities in Park Place along

This stormwater management report has been prepared by a professional engineer licensed in the State of Connecticut and provides a comprehensive evaluation of the fully developed Site as compared to existing (pre-developed) conditions. This report concludes that; drainage patterns will be generally maintained, there will be zero net increase in park flow rates discharging from the Site, and stormwater will be retained and treated to the maximum extent achievable in accordance with the 2024 Stormwater



DESCRIPTION OF EXISTING SITE

The existing 6.98-acre site is currently undeveloped. A review of historical aerial images confirms that the parcel has remained undeveloped since at least 1990. The 1934 aerial depicts the southern half of the site as cleared for apparent agricultural uses. The cleared areas are now revegetated and wooded.

TOPOGRAPHY - Natural topography of the parcel slopes from a high point along the northerly boundary in a south and southeasterly direction towards Park Place and West Main Street (Route 1). The northern half of the parcel has moderate to steep slopes ranging from 10% to 20%. The southern half of the parcel flattens into a topographic saddle with gentle to moderate slopes ranging from 2%

SOILS - The USDA NRCS Web Soil Survey depicts the Site within Charlton-Chatfield complex soils, very rocky, with slopes ranging from 0% to 45%. These soils are well drained with a Hydrologic Soil Group (HSG) rating of B. See Appendix C.

Deep observation pit testing was performed extensively over the site on three separate dates.

- Test pits 1 through 10 were performed in 2022 by Robert Pfanner, Jr. concentrated on the northerly wooded areas.
- Test pits 111 through 114 were performed in 2023 by Uncas Health District and Yantic River Consultants on the central wooded areas towards the toe of steeper slopes.
- Test pits D1 through D3 were performed in the southerly depression in the location of the proposed retention/detention basin. Witnessed soils consisted of topsoil to 6"-8", orange brown fine sandy loam to 28"-32", gray tan fine to medium sandy loam to 54"-88", and gray fine to medium sand and gravel slightly compact to 88"-96". Roots were witnessed 72" to 78" below grade with no clear indicator of seasonally high groundwater.

<u>VEGETATION</u> – The parcel is wooded with light to moderate undergrowth in southerly areas and moderate to dense undergrowth on the northerly steeper slopes.

<u>DRAINAGE</u> – Stormwater generally flows overland from the north to south on the parcel. Three drainage areas with distinct discharge points at the parcel property lines were identified based on topographic mapping and field confirmation.

- EX-01SW is 5.183 acres and encompasses the north and west portions of the Site with a discharge point at a low point along the southwesterly property line onto the rear yard of a property at 53 West Main Street.
- EX-02E is 1.389 acres and encompasses the southeastern corner of the Site with a discharge point in a depressed area along the easterly property line onto the rear yard of a property at 8 Park Place.
- EX-03S is 0.410 acres and encompasses the frontage portion of the Site with sheet flow discharge to the Park Place ROW.



STORMWATER MANAGEMENT

The following Standards were considered in the analysis and design.

SUMMARY OF APPLICABLE DESIGN CRITERIA

Hydrologic Design Criteria:

TR-55

Hydraulic Design Criteria:

CTDOT Drainage Manual

Climate Change Considerations:

CT DEEP Stormwater Quality Manual

Flood Hazard Areas:

N/A

Aquifer Protection Areas:

N/A

Treatment and Pollutant Removal:

CT DEEP Stormwater Quality Manual

Peak Flow Control Goal:

Zero Net Increase in Peak Flow from Site

SUMMARY OF LID TO REDUCE STORMWATER RUNOFF AND POLLUTANTS

Low Impact Development techniques were implemented to the maximum extent achievable prior to the consideration of structural stormwater best management practices (BMP) in accordance with the 2024 SQM. A list of LID techniques implemented into the design are provided below. It should be noted that as a conservative measure the design of the structural stormwater BMP does not take into consideration the hydrologic benefit of these measures.

- Minimize clearing: The limits of clearing shown are the minimum necessary to accommodate construction and provide adequate separation to each new building. Stumps will remain and native understory plants and shrubs preserved outside of the land disturbance footprint.
- Minimize building footprint: The multi-family building footprints have been reduced to the greatest extent possible while still achieving the purpose of the project.
- Minimize roadways, parking, and impervious surfaces: Parking quantities meet the minimum
- Preserving pre-development times of concentration to the maximum extent achievable.
- Use of low maintenance landscaping on perimeter areas.
- Disconnection of Impervious Surfaces:
 - Disconnection of all rear roof pitches through discharge to grade over vegetated areas.
 - Long and flat vegetated diversion swales to increase local flow path lengths and times
 - Vegetated depressions with elevation yard drain grates.
 - o Disconnection of impervious surfaces within stormwater collection system through



STRUCTURAL STORMATER BMP TREATMENT AND POLLUTANT REMOVAL

The design approach selected for the project consists of a multi-stage collection, treatment, retention, and attenuation system. The stages will consist of the following:

- Disconnect impervious surfaces to the maximum extent achievable prior to entering stormwater structural BMP.
- Install catch basin structures with minimum 2' sumps.
- First stage treatment: Discharge of stormwater from collections systems through sediment forebay capable of retaining a minimum of 25% of the water quality flow. Excess flows will bypass through a riprap filter berm and weir into the second stage treatment.
- Second stage treatment: Retain the Water Quality Volume (WQV) below the low-level orifice within the outlet structure to promote infiltration and recharge of groundwater for 90% of all storm events during a given year. The bottom of the basin will be excavated to elevation 25.00, which is 3'-4' below existing grade into the witnessed sandy loam soils. A minimal exfiltration rate of 0.3 in/hr was used in the analysis to confirm drain times of the retention area. The NRCS published exfiltration rate (hydraulic conductivity) of the existing sandy loam subsoils is 1.4 in/hr, therefore a quicker drain time and further reduction of peak flow rates is anticipated.
 - Final stage: Peak flow control through an outlet structure and weir plate to attenuate peak flow rates for the 1-year to 100-year storm events.

Tates	101 111				PRO	POSED TRE	ATME	VT	
AREA	DA	IA	WQV	WQF		Vol	Flow	Area	Note
Label	acre	acre	acre-ft	cfs	Method	0.059	N/A	N/A	25% WQV
PR-01SW	5.852	2.095	0.236	1.5	Sediment Forebay	0.339	N/A	N/A	144% WQV
	5.852	2.095	0.236	1.5	Retention	N/A	N/A	N/A	No Impervious
PR-01SW	0.627	0.000	0.000	0.0	N/A		N/A	N/A	Sheet Flow
PR-02E	_	0.120	0.014	0.1	Simple Disconnection	N/A	IVA	14/22	
PR-03S	0.504	0.120	U.U.T.	OT 17 1. D	ROPOSED TREATMENT SU	MMARY			

The proposed Stormwater Management System will retain the calculated WQV from the developed Site in accordance with the 2024 Stormwater Quality Manual.

PEAK FLOW CONTROL

Peak flow rates were calculated using TR-55 methodology. Hydrology Studio 2024 v.3.0.0.38 was used to generate peak flows with the following parameters for existing and proposed conditions:

DRAINAGE AREA: A description of the three drainage areas for existing Site and discharge points at the property lines are provided above. The proposed drainage areas were delineated based on proposed grading and drainage collection system routing. The same general discharge points were maintained for both existing and proposed conditions. See Appendix A for maps.

PR-01SW is 5.852 acres and encompasses the north and west portions of the developed Site with the same discharge point at a low point along the southwesterly property line. The retention and attenuation basin with stage-discharge outlet is located immediately prior to the discharge point.



- PR-02E is 0.627 acres and encompasses the undisturbed eastern corner of the Site with a discharge point in a depressed area along the easterly property line.
- PR-03S is 0.504 acres and encompasses the frontage portion of the developed Site with sheet flow discharge to the Park Place ROW.
- RAINFALL: Precipitation frequency and depth estimates (rainfall data) were obtained from NOAA Atlas 14, Volume 10, Version 3 at the Site geographic location. See Appendix C.
- CURVE NUMBER: Composite curve numbers (CN) were calculated based on the land cover types with consideration of the hydrologic soil groups and slopes. Based on USDA NRCS Web Soil Survey, soils within the subject watershed consist of HSG B.
- TIME OF CONCENTRATION: Time of concentrations (Tc) were estimated based on a review of topographic and surface runoff conditions for both existing and proposed conditions.

PEAK FLOW CALCULATIONS

A summary of flows (CFS) for existing and proposed conditions is provided below with a complete

M	-	A	REA (01 (SW)		A	REA (02 (E)	T A	REA (13 (8)	1				
STORM	EX	PR	DET	EX vs. PR	EX vs.	EX	PŖ	EX vs.	EX	PR	EX vs.	EX	PR	DET	E EX vs.	EX vs.
1	0.17	2.37	0.00	2.21	-0.17	0.05	0.03	PR			PR				PR	DET
2	0.52	3.68	0.18	3.16	-0.33	0.16	0.03	-0.02	0.01	0.15	0.14	0.22	2.54	0.17	2.32	-0.05
5	1.60	6.08	0.81	4.49	-0.79			-0.07	0.05	0.26	0.21	0.69	4.02	0.35	3.32	
10	2.86	8.27	1.35	5.41		0.52	0.29	-0.24	0.17	0.47	0.31	2.19	6.76	0.92		-0.34
25	4.91	11.37	3.64		-1.52	0.94	0.50	-0.45	0.30	0.67	0,37	3.96			4.57	-1.27
50	6.60			6.46	-1.27	1.60	0.83	-0.78	0.51	0.96	0.45		9.28	1.55	5.32	-2.41
-		13.77	5.20	7.17	-1.41	2.15	1.10	-1.06	0.68			6.76	12.88	4.09	6.12	-2.67
00	8.55	16.38	8.32	7.84	-0.23	2.78	1.40			1.18	0.50	9.08	15.67	5.82	6.59	-3.26
					TAI			-1.38 LOW C	0.88	1.43	0.55	11.74	18.74	9.15	7.00	-2.59

A comparison of peak flow control for each subarea and the entire Site is provided below:

AREA 01: Peak flow rates discharging to the southwest property line of the Site will be reduced for the 1-year to 100-year storm events. The decrease in peak flow rates can be attributed to the retention and attenuation provided by the proposed basin and outlet structure. The proposed basin fully retains the calculated water quality volume (1.3") and the 1-year storm event (2.87") without discharge.

AREA 02: Peak flow rates discharging to the eastern property line will be reduced for the 1-year to 100-year storm events due to the reduction in total area and minimal disturbance of existing

AREA 03: Peak flow rates discharging to the Park Place ROW will slightly increase for the 1-year

SITE: Overall peak flow rates discharging from the developed site will be reduced for the 1-year to 100-year storm events as compared to existing (pre-developed) conditions.



As described above, disconnection of impervious surfaces prior to the stormwater structural BMPs were not considered in the analysis as a conservative measure. As such, calculated peak flow rates for proposed conditions would likely be further reduced, in particular for more frequent storm events (< 2-year).

CONCLUSION

The proposed development and stormwater management system reduce peak flow rates discharging from the Site for the 1-year to 100-storm events, thereby meeting the zero net increase in stormwater runoff requirement. There are no anticipated adverse impacts on downstream properties or the Park Place ROW.

CONSTRUCTION EROSION AND SEDIMENT CONTROL

A plan to control construction related impacts, including erosion, sedimentation, and other pollutant sources has been prepared in accordance with the 2023 Connecticut Guidelines for Soil Erosion and Sediment Control. The Erosion and Sediment Control Plan is included in the submitted plan set.

OPERATION AND MAINTENANCE

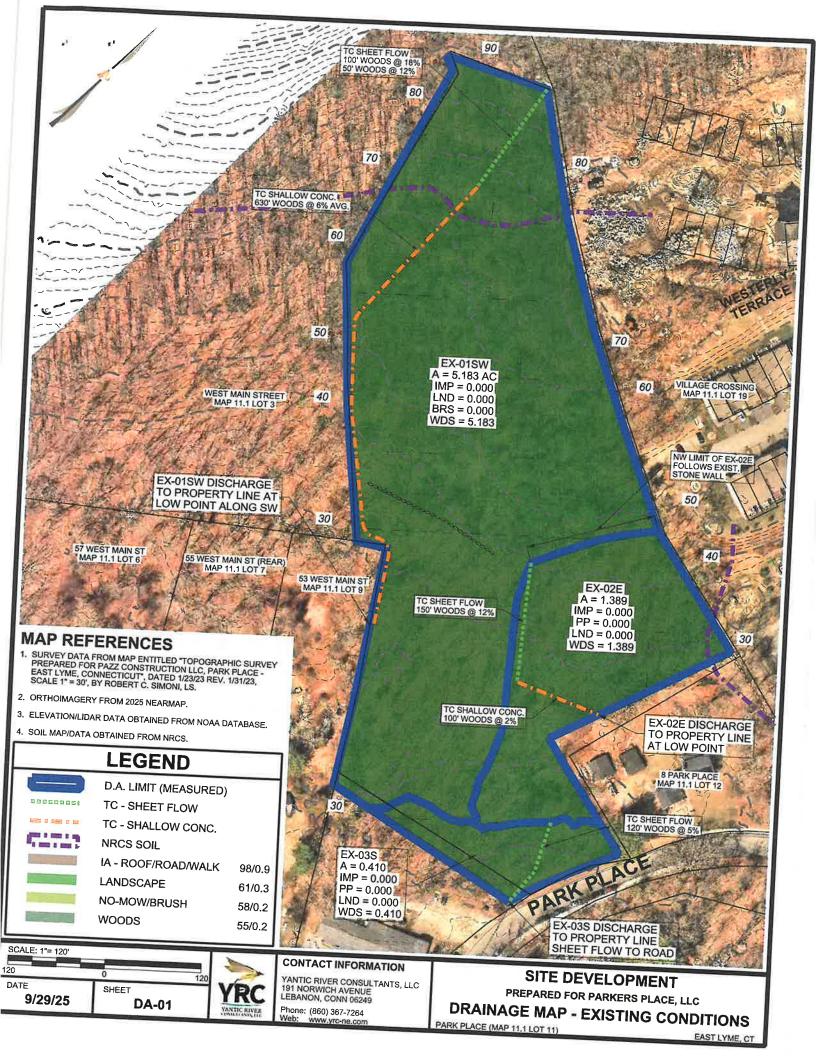
A long-term operation and maintenance plan has been developed to ensure that stormwater management systems function as designed. The O&M plan is provided on the Grading and Utility Plan as part of the submitted plan set.

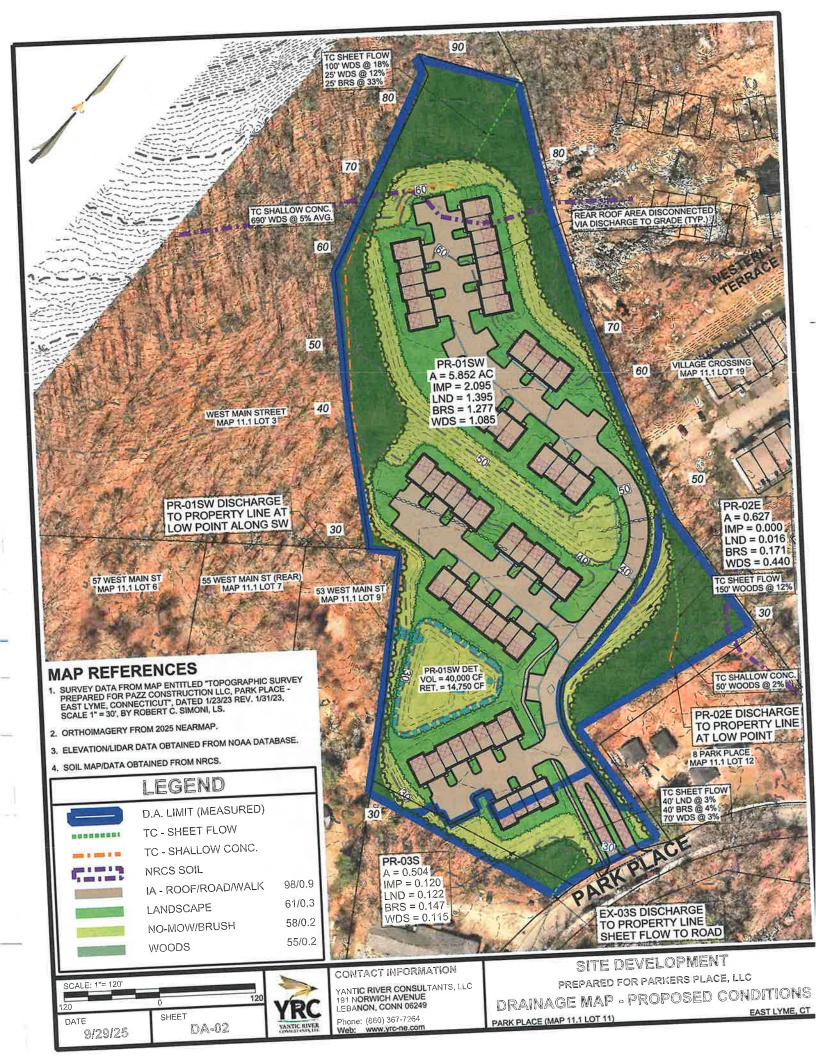


APPENDIX A DRAINAGE AREA MAPS

EXISTING CONDITIONS PROPOSED CONDITIONS

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APPENDIX B HYDROLOGIC COMPUTATIONS

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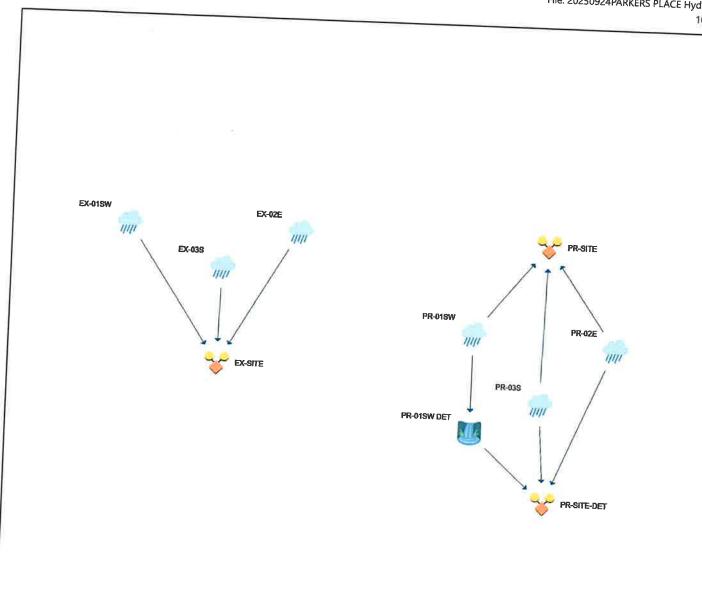
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Basin Model

Hydrology Studio v 3.0.0.38



Hydrograph by Return Period

File: 20250924PARKERS PLACE Hydrology.hys 10-06-2025

	udio v 3.0.0.38					Peak Outf	low (cfs)			
yd. lo.	Hydrograph Type	Hydrograph Name	1-yr	2-yr	3-уг	5-yr	10-yr	25-уг	50-yr	100-yr
-		EX-01SW	0.166	0.517		1.598	2.863	4.907	6.603	8.545
1	NRCS Runoff	EX-02E	0.046	0.157		0.520	0.942	1.603	2.154	2.784
2	NRCS Runoff	EX-03S	0.013	0.048		0.166	0.299	0.508	0.681	0.879
3	NRCS Runoff	EX-SITE	0.223	0.692		2.191	3.958	6.756	9.080	11.74
4	Junction	PR-01SW	2.371	3.680		6.083	8.268	11.37	13.77	16.38
5	NRCS Runoff	PR-02E	0.027	0.090		0.285	0.495	0.825	1.095	1.403
6	NRCS Runoff		0.150	0.260		0.472	0.670	0.958	1.183	1.432
7	NRCS Runoff	PR-03S	2.542	4.015		6.762	9.275	12.88	15.67	18.74
8	Junction	PR-SITE	0.000	0.184		0.809	1.346	3.636	5.198	8.316
9	Pond Route	PR-01SW DET PR-SITE-DET	0.172	0.351		0.921	1.550	4.085	5.816	9.147

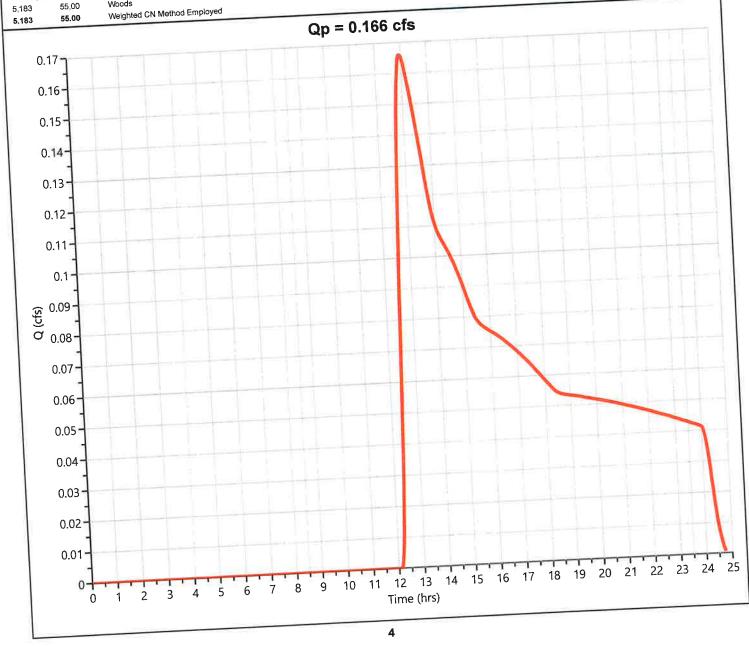
NRCS Runoff EX-015W 0.166 12.93 3.061	Hyd. No.	Hydrograph Type	Hydrograph Name	Peak Flow	Time to Peak	Hydrograph Volume	Inflow Hyd(s)	0924PARKERS PL	10-06
2 NRCS Runoff EX-02E 0.046 12.70 823	1	NRCS Runoff	EX-01SW			(cuft)	riyu(s)	(ft)	Storage
3 NRCS Runoff EX-03S 0.013 12.63 238	2	NRCS Runoff	EX-02E			3,061			1
4 Junction EX-SITE 0.013 12.63 238 5 NRCS Runoff PR-01SW 2.371 12.43 16,019 6 NRCS Runoff PR-02E 0.027 12.55 413	3	NRCS Runoff	EX-03S			823			
5 NRCS Runoff PR-01SW 2.371 12.92 4,121 1,2,3 6 NRCS Runoff PR-02E 0.027 12.55 413 — 7 NRCS Runoff PR-03S 0.150 12.37 1,003 — 8 Junction PR-SITE 2.542 12.43 17,434 5,6,7 9 Pond Route PR-01SW DET 0.000 11.93 0.000 5 27.89 14,012 10 Junction PR-SITE-DET 0.172 12.43 1.012	4	Junction	1			238	2000		1
6 NRCS Runoff PR-02E 2.371 12.43 16,019 — 7 NRCS Runoff PR-03S 0.027 12.55 413 — 8 Junction PR-SITE 2.542 12.43 1,003 — 9 Pond Route PR-01SW DET 0.000 11.93 0.000 5 27.89 14,012 10 Junction PR-SITE-DET 0.172 12.43 1.012	5	NRCS Runoff			12.92	4,121	1, 2, 3		
7 NRCS Runoff PR-03S 0.027 12.55 413 -	6	NRCS Runoff	1		12.43	16,019			
8 Junction PR-SITE 2.542 12.43 17,434 5, 6, 7 10 Junction PR-SITE-DET 0.172 12.43 1.003 1.0	7				12.55	413			
9 Pond Route PR-01SW DET 0.000 11.93 0.000 5 27.89 14,012	8			0.150	12.37	1,003			
10 Junction PR-SITE-DET 0.000 11.93 0.000 5 27.89 14,012	9			2.542	12.43	17,434			V.
PR-SITE-DET 0.172 12.42 14.012	10			0.000	11.93	0.000		27.00	
	.	Junction	PR-SITE-DET	0.172	12.42			27.89	14,012

Hyd. No. 1 EX-01SW

.X-01011			- 100 5
		Peak Flow	= 0.166 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.93 hrs
Storm Frequency	= 1-yr	Runoff Volume	= 3,061 cuft
Time Interval	= 1 min	Curve Number	= 55.00*
Drainage Area	= 5.183 ac	Time of Conc. (Tc)	= 31.45 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOAA-D
Total Rainfall	= 2.87 in	Shape Factor	= 484
Storm Duration	= 24 hrs	Cp	

* Composite CN Worksheet

DESCRIPTION AREA (ac) CN Woods 55.00



10-06-2025

EX-01SW NRCS Runoff

Description		Segments		
Description	A	В	C	Tc (min)
Sheet Flow				
Description	Woods	Woods		
Manning's n	0.400	0.400	0.013	
Flow Length (ft)	100	50		
2-yr, 24-hr Precip. (in)	3.44	3.44	3.44	
Land Slope (%)	18	12		
Travel Time (min)	8.60	5.81	0.00	14.41
Shallow Concentrated Flow				
Flow Length (ft)	630			
Watercourse Slope (%)	6.00	0.00	0.00	
Surface Description	Forest	Paved	Paved	
Average Velocity (ft/s)	.62			
Travel Time (min)	17.04	0.00	0.00	17.04
Channel Flow				
X-sectional Flow Area (sqft)				
Wetted Perimeter (ft)				
Channel Slope (%)				
Manning's n	0.013	0.013	0.013	
Velocity (ft/s)				
Flow Length (ft)				
Travel Time (min)	0.00	0.00	0.00	0.00
Total Travel Time				31.45 mi

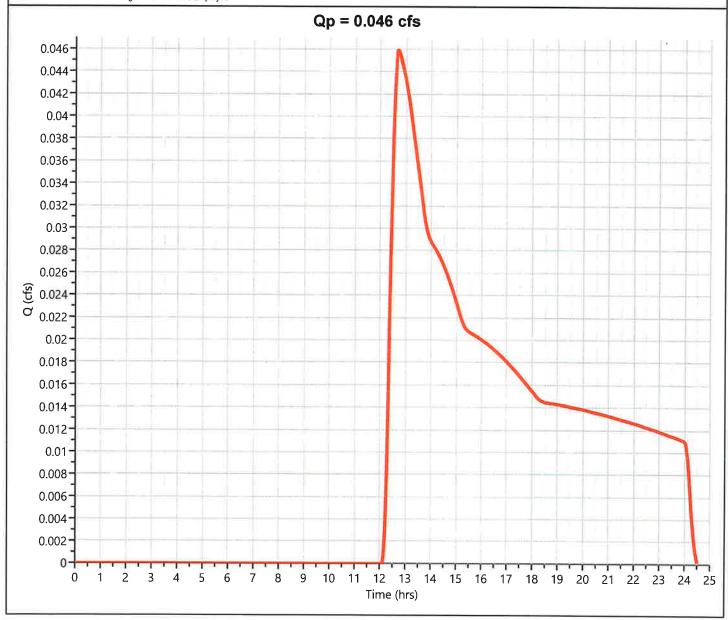
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.046 cfs
Storm Frequency	= 1-yr	Time to Peak	= 12.70 hrs
Time Interval	= 1 min	Runoff Volume	= 823 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 2.87 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55,00 Woods

1.389 55.00 Weighted CN Method Employed



10-06-2025

EX-02E NRCS Runoff

Description		Segments		
	A	В	С	To feet
				Tc (min
Sheet Flow				
Description	Woods	Woods		
Manning's n	0.400	0.400	0.040	
Flow Length (ft)	100	50	0.013	
2-yr, 24-hr Precip. (in)	3.44	3.44		
Land Slope (%)	12	12	3.44	
Travel Time (min)	10.11	5.81	0.00	15.92
Shallow Concentrated Flow				
Flow Length (ft)	100			
Watercourse Slope (%)	2.00			
Surface Description		0.00	0.00	
Average Velocity (ft/s)	Forest	Paved	Paved	
(lus)	.36			
Travel Time (min)	4.68	0.00	0.00	4.68
Channel Flow				
X-sectional Flow Area (sqft)				
Wetted Perimeter (ft)				
Channel Slope (%)				
Manning's n	0.040			
Velocity (ft/s)	0.013	0.013	0.013	
Flow Length (ft)				
Travel Time (min)	0.00	0.00	0.00	0.00
Total Travel Time				0.00
.our Havel Inne				20.61 min

Hyd. No. 3 **EX-03S**

		Peak Flow	= 0.013 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.63 hrs
Storm Frequency	= 1-yr	Runoff Volume	= 238 cuft
Time Interval	= 1 min	Curve Number	= 55.00*
Drainage Area	= 0.41 ac	Time of Conc. (Tc)	= 18.32 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOAA-D
Total Rainfall	= 2.87 in	Shape Factor	= 484
Storm Duration	= 24 hrs	Griape i deter	

* Composite CN Worksheet

0.002

0.001

DESCRIPTION AREA (ac) CN 55.00 Woods

Weighted CN Method Employed 0.41 55.00 Qp = 0.013 cfs0.014-0.013 0.012-0.011 0.01 0.009 0.008 (\$\frac{5}{0}\) 0.007 0.006 0.005 0.004 0.003

Time (hrs)

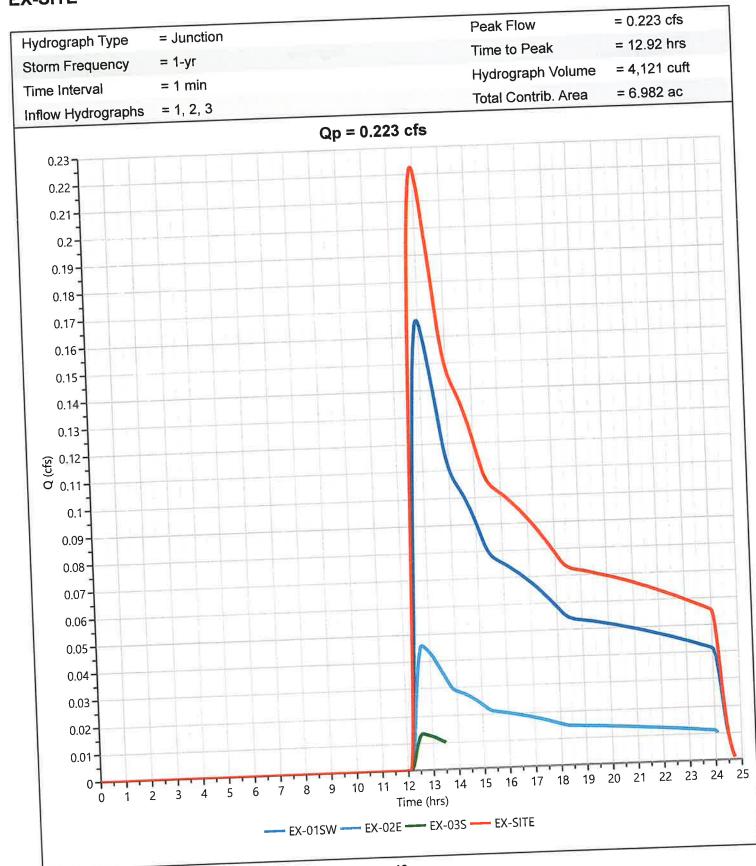
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25

10-06-2025

EX-03S NRCS Runoff

	Segments		
A	В	C	Tc (min
			10 (11111)
Woods	Woods		
0.400	0.400	0.013	
100	20	0.010	
3.44	3.44	2 44	
5	5	3.44	
14.36	3.96	0.00	18.32
0.00			
		0.00	
i aved	Paved	Paved	
0.00	0.00	0.00	0.00
0.013	0.045		
0.010	0.013	0.013	
0.00	0.00	0.00	0.00
	Woods 0.400 100 3.44 5 14.36 0.00 Paved 0.00	Woods 0.400 0.400 100 20 3.44 3.44 5 5 14.36 3.96 0.00 Paved Paved 0.00 0.00 0.00	Woods Woods 0.400 0.400 0.013 100 20 3.44 3.44 5 5 14.36 3.96 0.00 0.00 0.00 0.00 Paved Paved 0.00 0.00 0.00 0.013 0.013 0.013 0.00 0.00 0.003

EX-SITE

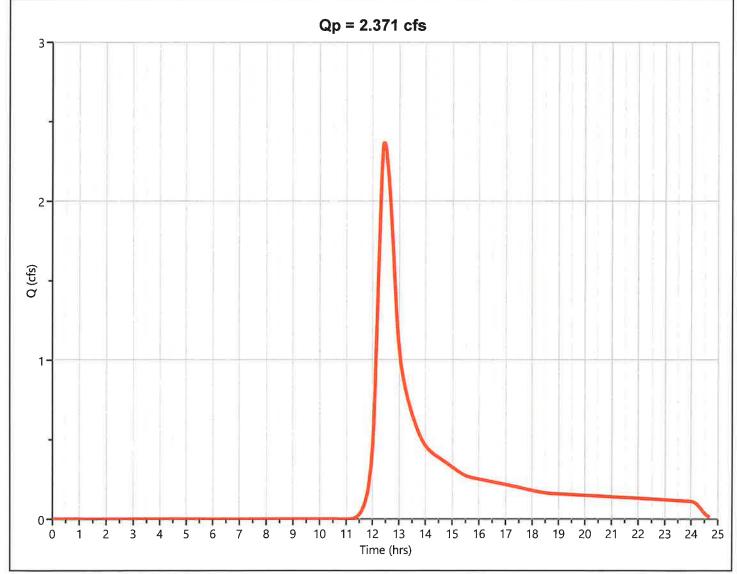


PR-01SW Hyd. No. 5

Hydrograph Type	= NRCS Runoff	Peak Flow	= 2.371 cfs
Storm Frequency	= 1-yr	Time to Peak	= 12.43 hrs
Time Interval	= 1 min	Runoff Volume	= 16,019 cuft
Drainage Area	= 5.852 ac	Curve Number	= 72.48*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 34.6 min
Total Rainfall	= 2.87 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
2.095	98.00	Impervious
1.395	61.00	Landscape
1.277	58.00	Conservation
1.085	55.00	Woods
5.852	72.48	Weighted CN Method Employed



10-06-2025

PR-01SW NRCS Runoff

Description		Segments		
Description	ay domes A	В	C -	Tc (min)
	The same wife	Survey of Carlo	1498,884 ::	
Sheet Flow				
Description	Woods	Woods	Conservation	
Manning's n	0.400	0.400	0.400	
Flow Length (ft)	100	25	25	
2-yr, 24-hr Precip. (in)	3.44	3.44	3.44	
Land Slope (%)	18	12	33	
Travel Time (min)	8.60	3.34	2.23	14.16
Shallow Concentrated Flow				
Flow Length (ft)	690			
Watercourse Slope (%)	5.00	0.00	0.00	
Surface Description	Forest	Paved	Paved	
Average Velocity (ft/s)	.56			
Travel Time (min)	20.44	0.00	0.00	20.44
Channel Flow				
X-sectional Flow Area (sqft)				
Wetted Perimeter (ft)				
Channel Slope (%)				
Manning's n	0.013	0.013	0.013	
Velocity (ft/s)				
Flow Length (ft)				
Travel Time (min)	0.00	0.00	0.00	0.00
Total Travel Time				34.6 mir

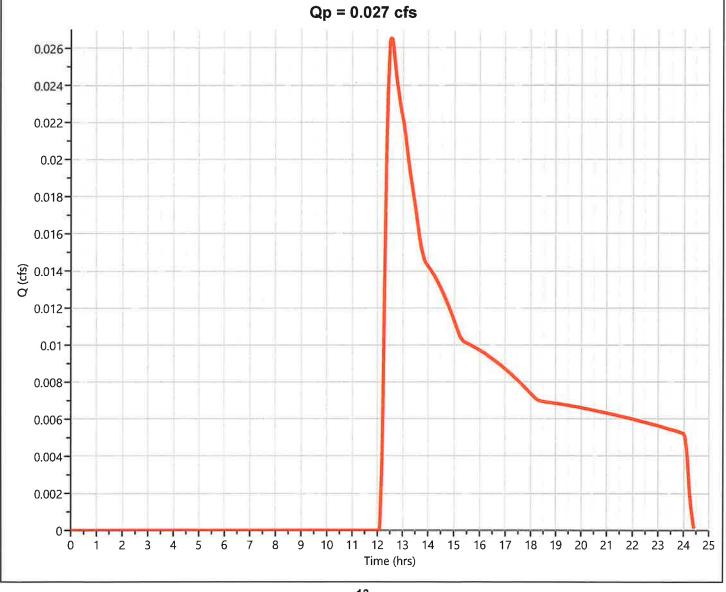
PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.027 cfs
Storm Frequency	= 1-yr	Time to Peak	= 12.55 hrs
Time Interval	= 1 min	Runoff Volume	= 413 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 2.87 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0.016	61.00	Landscape
0.171	58,00	Conservation
0.44	55.00	Woods

0.627 55.97 Weighted CN Method Employed



10-06-2025

PR-02E NRCS Runoff

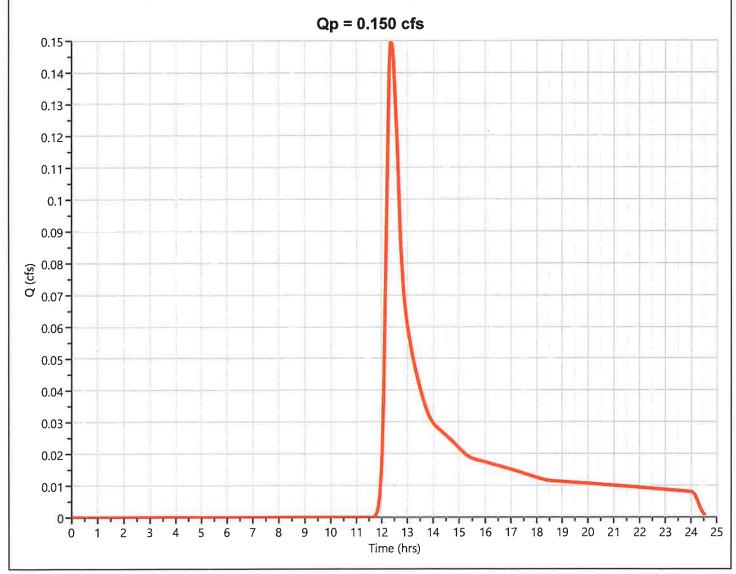
Description		Segments		
Description	A Punellips	В	ALL C	Tc (min)
Sheet Flow	to smill	Oak Sh	Company of Control	
Description	Woods	Woods		
Manning's n	0.400	0.400	0.013	
Flow Length (ft)	100	50		
2-yr, 24-hr Precip. (in)	3.44	3.44	3.44	
Land Slope (%)	12	12		
Travel Time (min)	10.11	5.81	0.00	15.92
Shallow Concentrated Flow				
Flow Length (ft)	50			
Watercourse Slope (%)	2.00	0.00	0.00	
Surface Description	Forest	Paved	Paved	
Average Velocity (ft/s)	.36			
Travel Time (min)	2.34	0.00	0.00	2.34
Channel Flow				
X-sectional Flow Area (sqft)				
Wetted Perimeter (ft)				
Channel Slope (%)				
Manning's n	0.013	0.013	0.013	
Velocity (ft/s)				
Flow Length (ft)				
Travel Time (min)	0.00	0.00	0.00	0.00
Total Travel Time				18.27 mir

PR-03S Hyd. No. 7

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.150 cfs
Storm Frequency	= 1-yr	Time to Peak	= 12.37 hrs
Time Interval	= 1 min	Runoff Volume	= 1,003 cuft
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Total Rainfall	= 2.87 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0.12	98.00	Impervious
0.122	61.00	Landscape
0.147	58.00	Conservation
0.115	55.00	Woods
0.504	67 57	Weighted CN Method Emp



10-06-2025

PR-03S NRCS Runoff

Description		Segments		
	A Physical A	В	C	Tc (min)
Sheet Flow	Time of	6 material (349.)		
Description	Landscape	Conservation	Woods	
Manning's n	0.240	0.400	0.400	
Flow Length (ft)	40	40	70	
2-yr, 24-hr Precip. (in)	3.44	3.44	3.44	
Land Slope (%)	3	4	3	
Travel Time (min)	5.62	7.54	13.24	26.40
Shallow Concentrated Flow				
Flow Length (ft)				
Watercourse Slope (%)	0.00	0.00	0.00	
Surface Description	Paved	Paved	Paved	
Average Velocity (ft/s)				
Travel Time (min)	0.00	0.00	0.00	0.00
Channel Flow				
X-sectional Flow Area (sqft)				
Wetted Perimeter (ft)				
Channel Slope (%)				
Manning's n	0.013	0.013	0.013	
Velocity (ft/s)				
Flow Length (ft)				
Travel Time (min)	0.00	0.00	0.00	0.00
Total Travel Time				26.4 min

PR-SITE Hyd. No. 8

-lydrograph Type	= Junction		Peak Flow	= 2.542 cfs
Storm Frequency	= 1-yr		Time to Peak	= 12.43 hrs
Time Interval	= 1 min		Hydrograph Volume	= 17,434 cuft
nflow Hydrographs	= 5, 6, 7		Total Contrib. Area	= 6.983 ac
		Qp = 2.542 cfs		
37				
1				
2-				
(cr) 7				
7				
1				
		11		
0 1 2 3	4 5 6 7 8	9 10 11 12 13 14 15	5 16 17 18 19 20	21 22 23 24 2
0 1 2 3	4 5 6 7 6	Time (hrs)	, , , , , , , , , , , , , , , , , , , ,	
	PR-0	1SW	PR-SITE	

PR-01SW DET

Hyd. No. 9

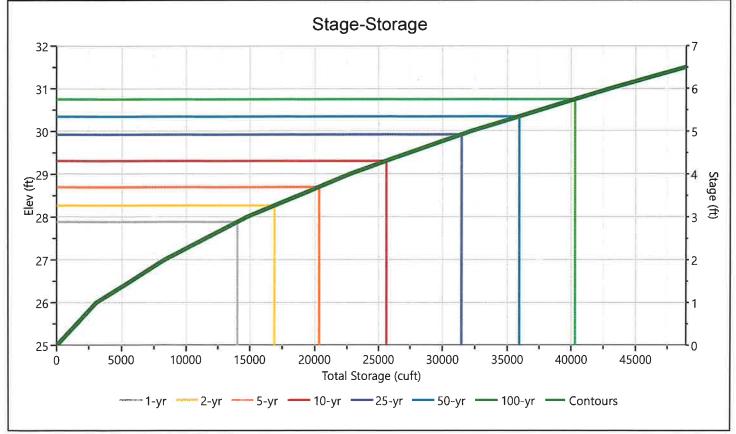
lydrograph Type	= Pond Route	Peak Flow	= 0.000 cfs	
Storm Fréquency	= 1-yr	Time to Peak	= 11.93 hrs	
îme Interval	= 1 min	Hydrograph Volume	= 0.000 cuft	
nflow Hydrograph	= 5 - PR-01SW	Max. Elevation	= 27.89 ft = 14,012 cuft	
ond Name	= PR-01 DETENTION	Max. Storage		
ond Routing by Storage	ndication Method		_	
	Qp = 0.000 c	fs		
3				
1				
2-				
a				
1-				
-				
0				
0 1	2 3 4 5 6	7 8 9 1	0 11	
	Time (hrs)			
	— PR-01SW — PR-0	ISW DET		

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PR-01 DETENTION

Stage-Storage

User Defined Contour	Stage / Storage Table						
Description	Input	Stage (ft)	Elevation (ft)	Contour Area (sqft)	Incr. Storage (cuft)	Total Storage (cuft)	
Bottom Elevation, ft	25.00						
\\\-id= (0\)	100.00	0.00	25.00	1,780	0.000	0.000	
Voids (%)	100.00	1.00	26.00	4,600	3,080	3,080	
Volume Calc	Conic	2.00	27.00	5,790	5,183	8,263	
		3.00	28.00	7,200	6,482	14,745	
		4.00	29.00	8,740	7,957	22,702	
		5.00	30.00	10,250	9,484	32,186	
		6.00	31.00	11,480	10,858	43,044	
		6.50	31.50	12,140	5,904	48,947	

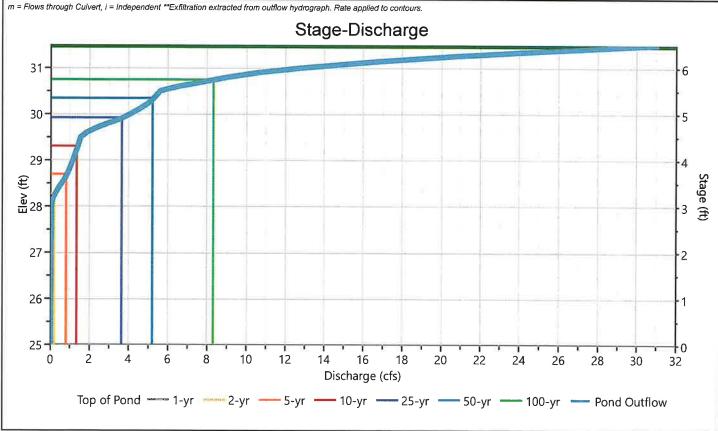


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PR-01 DETENTION

Stage-Discharge

Culvert / Orifices	Cir Culusum		Orifice	O-ifi a F		
Culvert / Offices	Cir Culvert	1 (m)	2 3 (m)		Orifice Plate	
Rise, in	15	8	9	4	Orifice Dia, in	
Span, in	15	8	9	36	No. Orifices	
No. Barrels	1	1	2	1	Invert Elevation, ft	
Invert Elevation, ft	28.00	28.00	28.75	29.50	Height, ft	
Orifice Coefficient, Co	0.60	0.60	0.60	0.60	Orifice Coefficient, Co	
Length, ft	25					
Barrel Slope, %	.5					
N-Value, n	0.013				T I THE STATE	
Weirs	Riser		Weir		Ancillone	
VVCII 5	Riser	1 (i)	2	3	Ancillary	
Shape / Type	Box	Broad Crested			Exfiltration, in/hr	0.30**
Crest Elevation, ft	30.5	30.75				
Crest Length, ft	14	8				
Angle, deg		18.4 (3:1)			TO SECTION AND	
Weir Coefficient, Cw	3.3	3.3			The same of the same	



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10-06-2025

PR-01 DETENTION

Stage-Storage-Discharge Summary

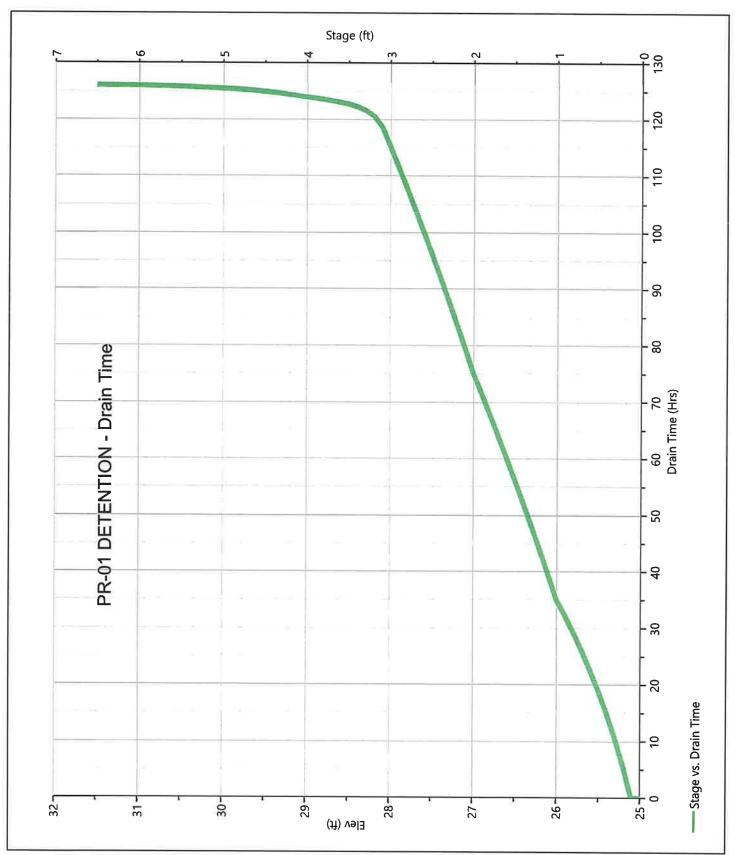
	ser Total	User	Exfil	Pf Riser		Weirs, cfs		Riser	s	Orifices, cf	C	Culvert	Storage	Elev.	Stage
1.00 26.00 3,080 0.001 0.001	fs) (cfs)	(cfs)			3	2	1		3	2	1				(ft)
2.00 27.00 8,263 0.000 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.000	0.000		0.000				0.000	0.000	0.000	0.000	0.000	0.000	0.000	25.00	0.00
3.00 28.00 14,745 0.000 0.000 0.000 0.000 0.000 0.000 0.000 4.00 29.00 22,702 1.094 oc 1.094 0.000 0.000 0.000 0.000 0.000 5.00 30.00 32,186 4.005 oc 1.225 0.000 2.780 0.000 0.000 0.000 6.00 31.00 43,044 9.105 ic 0.000 0.000 0.000 3.548 0.080	0.032		0.032				0.000	0.000	0.000	0.000	0.000	0.000	3,080	26.00	1.00
4.00 29.00 22,702 1.094 oc 1.094 0.000 0.000 0.000 0.000 0.000 5.00 30.00 32,186 4.005 oc 1.225 0.000 2.780 0.000 0.000 0.000 0.071 6.00 31.00 43,044 9.105 ic 0.000 0.000 0.000 3.548 0.080	0.040		0.040				0.000	0.000	0.000	0.000	0.000	0.000	8,263	27.00	2.00
5.00 30.00 32,186 4.005 oc 1.225 0.000 2.780 0.000 0.000 0.000 6.00 31.00 43,044 9.105 ic 0.000 0.000 0.000 3.548 0.080	0.050		0.050				0.000	0.000	0.000	0.000	0.000	0.000	14,745	28.00	3.00
6.00 31.00 43,044 9.105 ic 0.000 0.000 0.000 3.548 0.080	1.155		0.061				0.000	0.000	0.000	0.000	1.094	1.094 oc	22,702	29.00	4.00
	4.076		0.071				0.000	0.000	2.780	0.000	1.225	4.005 oc	32,186	30.00	5.00
6.50 31.50 48,947 10.02 ic 0.000 0.000 0.000 21.01 0.000 0.084 0 0.084 0 0.000	12.73		0.080				3.548	0.000	0.000	0.000	0.000	9.105 ic	43,044	31.00	6.00
	31.11		0.084				21.01	0.000	0.000	0.000	0.000	10.02 ic	48,947	31.50	6.50
						0)									
													(

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10-06-2025

PR-01 DETENTION

Pond Drawdown



PR-SITE-DET Hyd. No. 10

Hydrograph Type	= Junction				Peal	c Flow	= 0.172	cfs
Storm Frequency	= 1-уг				Time	to Peak	= 12.42	hrs
Time Interval	= 1 min				Hydi	ograph Volume	= 1,415	cuft
nflow Hydrographs	= 6, 7				Tota	Contrib. Area	= 1.131	ac
			Qp = 0	.172 cfs				
0.18				111			IV U	
0.17				1				Him
0.16							4-44	
0.15								
-				A				1-11
0.14								- 11
0.13							77	
0.12								
0.11								
0.1								
O.09								
0.08								
0.07				-1-11				
0.06								
4								
0.05								
0.04				1 (
0.03					1			
0.02					1			
3								
0.01								1
0 1 2	3 4 5 6	7 8	9 10 11	12 13 14	15 16	17 18 19 20	21 22 2	23 24
				Time (hrs)				

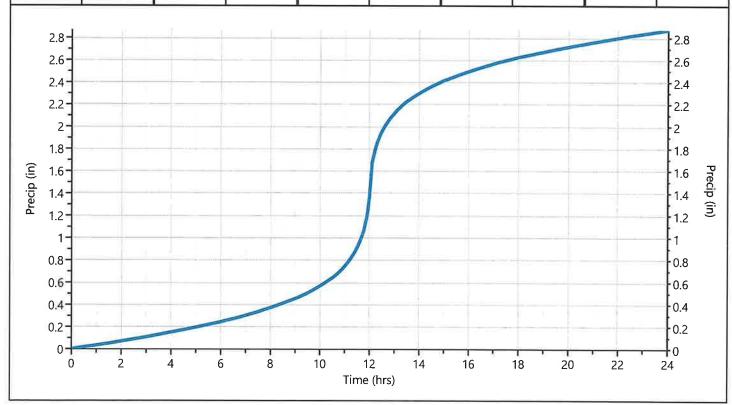
Design Storm Report

Hydrology Studio v 3.0.0.38 10-06-2025

Storm Distribution: NOAA-D, 24-hr

Storm		Total Rainfall Volume (in)								
Duration	✓ 1-yr	2-yr	3-yr	5-уг	10-уг	25-уг	50-yr	100-yr		
24 hrs	2.87	3.44	0.00	4.38	5.17	6.24	7.04	7.90		

			Incre	mental Raint	all Distribution	, 1-yr			
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
11.60	0.008658	11.78	0.012499	11.97	0.029919	12.15	0.017344	12.33	0.009113
11.62	0.009112	11.80	0.012500	11.98	0.029921	12.17	0.017344	12.35	0.009112
11.63	0.009112	11.82	0.017344	12.00	0.029918	12,18	0.017345	12.37	0.009113
11.65	0.009113	11.83	0.017345	12.02	0.049922	12.20	0.017344	12.38	0.009112
11.67	0.009112	11.85	0.017344	12.03	0.049925	12.22	0.012499	12.40	0.009113
11.68	0.009113	11.87	0.017344	12.05	0.049922	12.23	0.012499	12.42	0.008658
11.70	0.009112	11.88	0.017345	12.07	0.049925	12.25	0.012499	12.43	0.008658
11.72	0.012499	11.90	0.017344	12.08	0.049922	12.27	0.012499	12.45	0.008658
11.73	0.012499	11.92	0.029920	12.10	0.049925	12.28	0.012499	12.47	0.008658
11.75	0.012499	11.93	0.029919	12.12	0.017344	12.30	0.012498	12.48	0.008658
11.77	0.012499	11.95	0.029921	12.13	0.017345	12,32	0.009112	12.50	0.008658
					. I				I



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Hydrograph 2-yr Summary

yd. Hydrograph o. Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation (ft)	Maximum Storage (cuft)
1 NRCS Runoff	EX-01SW	0.517	12.67	6,169	1 8707 21		
2 NRCS Runoff	EX-02E	0.157	12.47	1,658			
3 NRCS Runoff	EX-03S	0.048	12.38	479	(2122)		
4 Junction	EX-SITE	0.692	12.58	8,307	1, 2, 3		
5 NRCS Runoff	PR-01SW	3.680	12.43	23,565			
6 NRCS Runoff	PR-02E	0.090	12.37	806	:		
7 NRCS Runoff	PR-03S	0.260	12.35	1,558			
8 Junction	PR-SITE	4.015	12.43	25,929	5, 6, 7		
9 Pond Route	PR-01SW DET	0.184	18.20	5,503	5	28.27	16,889
10 Junction	PR-SITE-DET	0.351	12.35	7,866	6, 7, 9		

EX-01SW

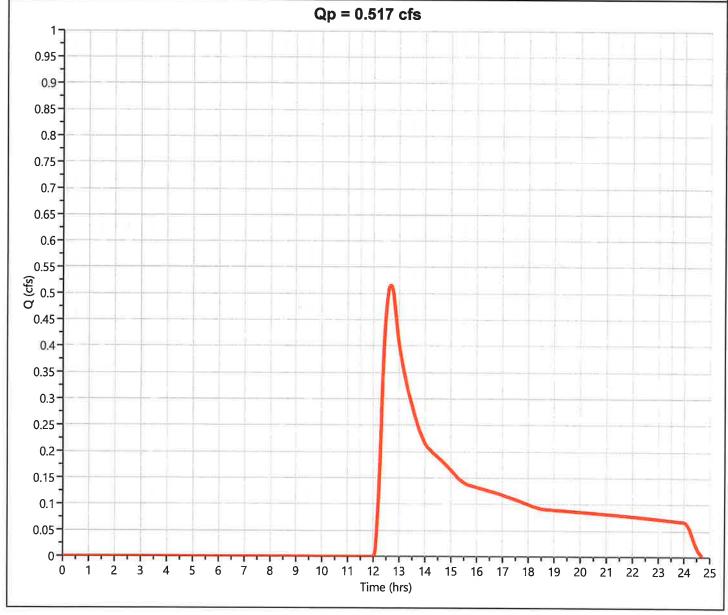
Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.517 cfs
Storm Frequency	= 2-yr	Time to Peak	= 12.67 hrs
Time Interval	= 1 min	Runoff Volume	= 6,169 cuft
Drainage Area	= 5.183 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 31.45 min
Total Rainfall	= 3.44 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 5.183 55,00 Woods

Weighted CN Method Employed 5.183 55.00



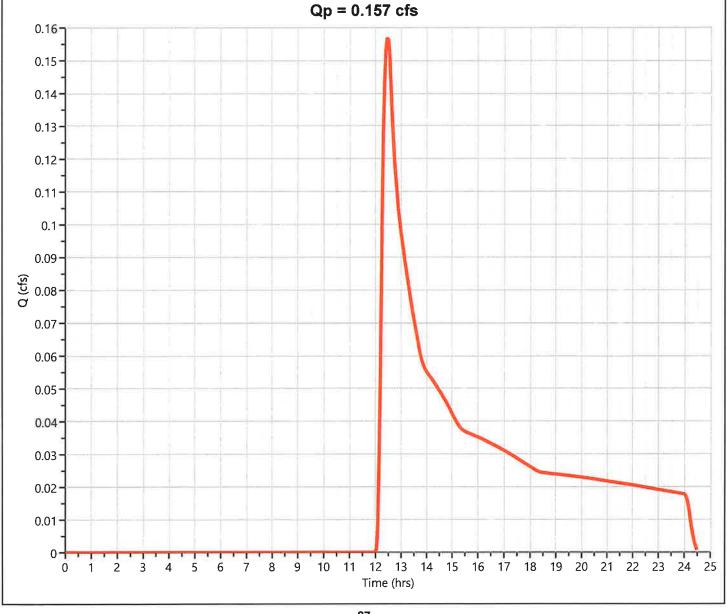
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.157 cfs
Storm Frequency	= 2-yr	Time to Peak	= 12.47 hrs
Time Interval	= 1 min	Runoff Volume	= 1,658 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 3.44 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55.00 Woods

1.389 55.00 Weighted CN Method Employed



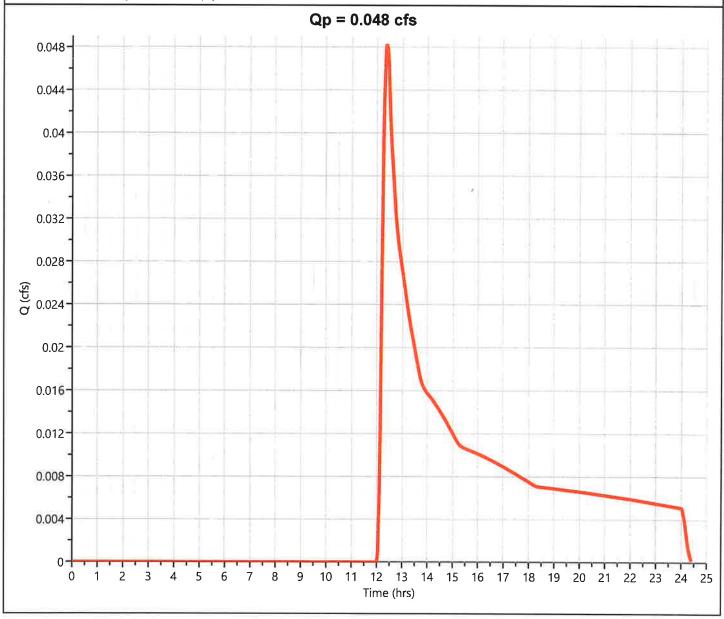
EX-03S Hyd. No. 3

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.048 cfs
Storm Frequency	= 2-yr	Time to Peak	= 12.38 hrs
Time Interval	= 1 min	Runoff Volume	= 479 cuft
Drainage Area	= 0.41 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.32 min
Total Rainfall	= 3.44 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

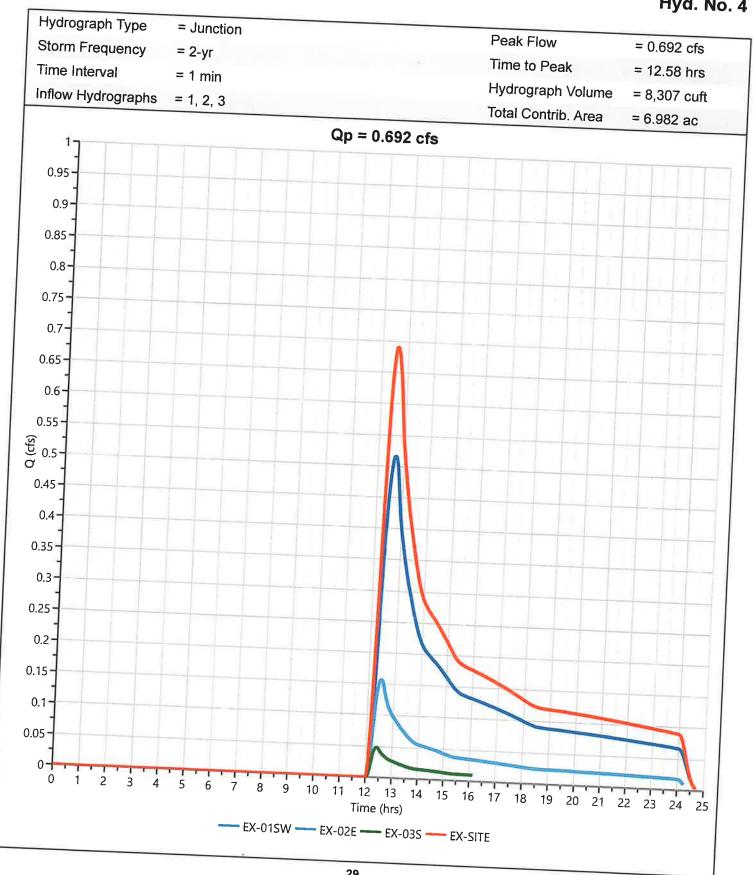
AREA (ac) CN DESCRIPTION 0.41 55.00 Woods

0.41 55.00 Weighted CN Method Employed



EX-SITE

Hyd. No. 4

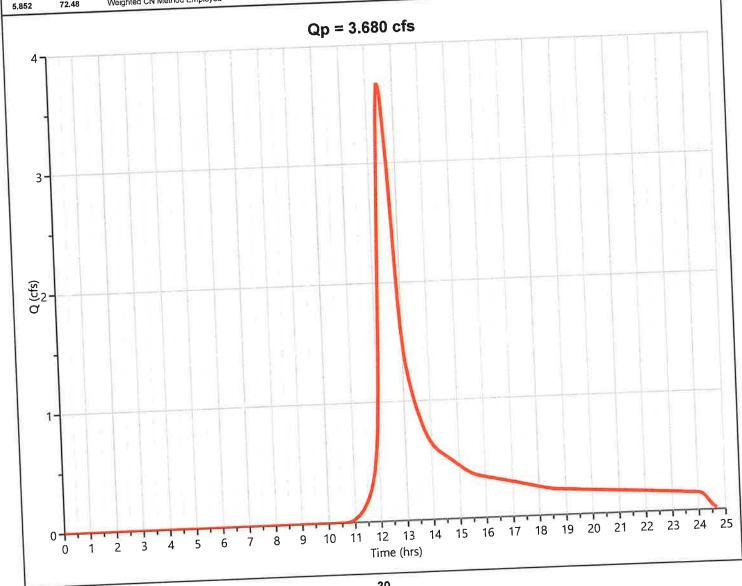


Hyd. No. 5

PR-01SW

		Peak Flow	= 3.680 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.43 hrs
Storm Frequency	= 2-yr	Runoff Volume	= 23,565 cuft
Time Interval	= 1 min	Curve Number	= 72.48*
Drainage Area	= 5.852 ac	Time of Conc. (Tc)	= 34.6 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOAA-D
Total Rainfall	= 3.44 in	Shape Factor	= 484
Storm Duration	= 24 hrs	Snape Factor	

AREA (ac)	CN	DESCRIPTION
2.095	98,00	Impervious
1.395	61,00	Landscape
1.277	58.00	Conservation
1.085	55,00	Woods
5.852	72.48	Weighted CN Method Employed

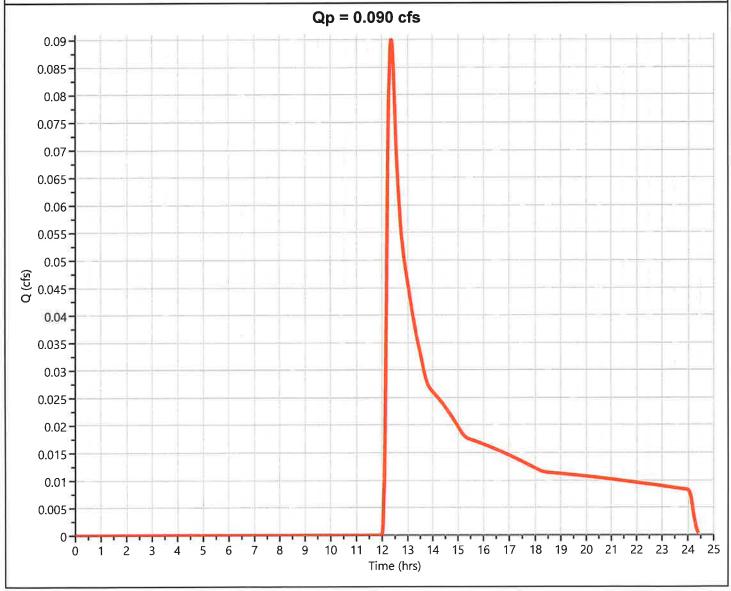




PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.090 cfs
Storm Frequency	= 2-yr	Time to Peak	= 12.37 hrs
Time Interval	= 1 min	Runoff Volume	= 806 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 3.44 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

AREA (ac)	CN	DESCRIPTION
0.016	61.00	Landscape
0.171	58.00	Conservation
0.44	55.00	Woods
0.627	55.97	Weighted CN Method Employed

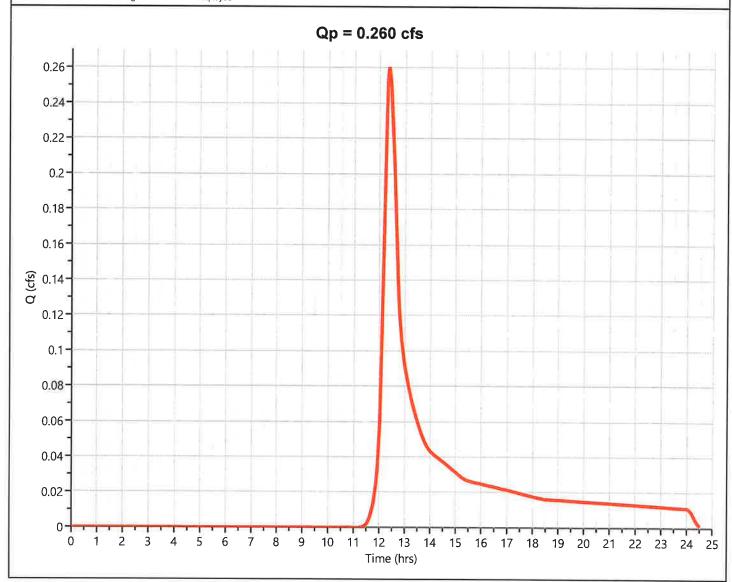


PR-03S

Hyd. No. 7

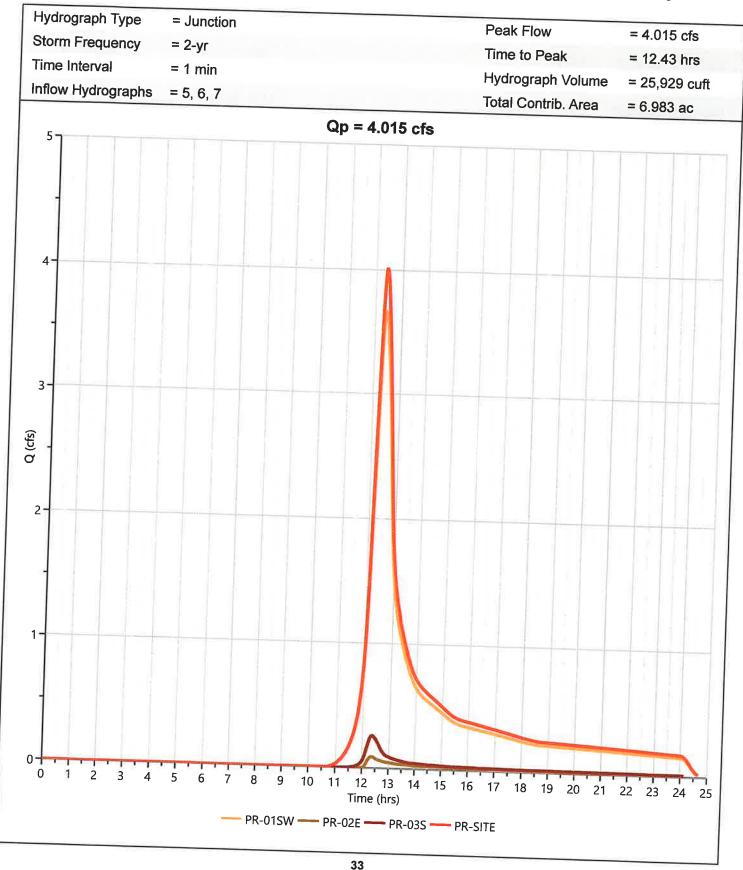
Storm Duration	= 24 hrs	Shape Factor	= 484
Total Rainfall	= 3.44 in	Design Storm	= NOAA-D
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Time Interval	= 1 min	Runoff Volume	= 1,558 cuft
Storm Frequency	= 2-yr	Time to Peak	= 12.35 hrs
Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.260 cfs

AREA (ac)	CN	DESCRIPTION
0_12	98.00	Impervious
0.122	61.00	Landscape
0_147	58.00	Conservation
0.115	55.00	Woods
0.504	67.57	Weighted CN Method Employed



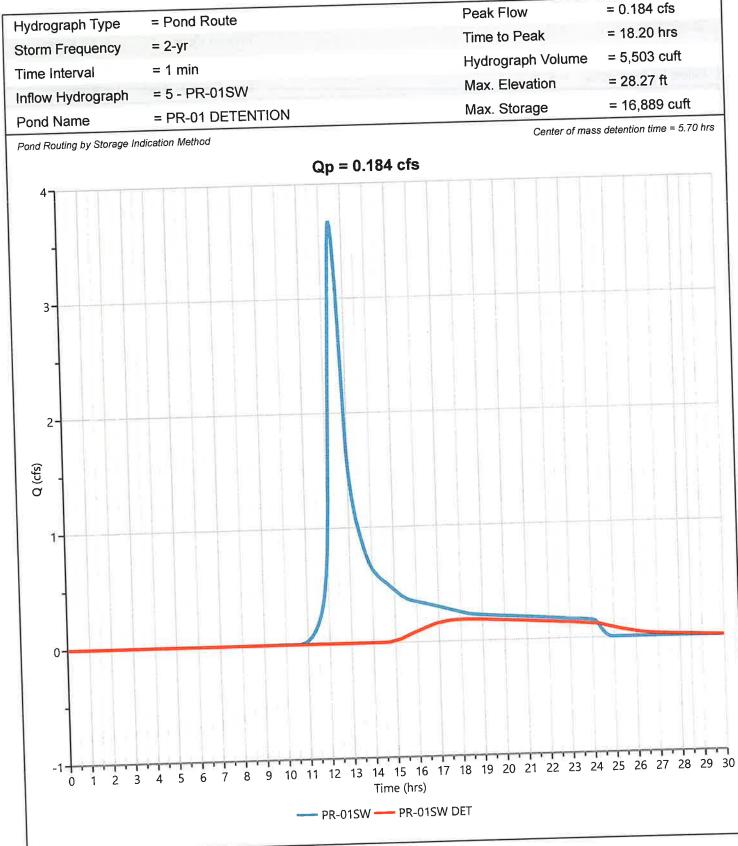
PR-SITE

Hyd. No. 8



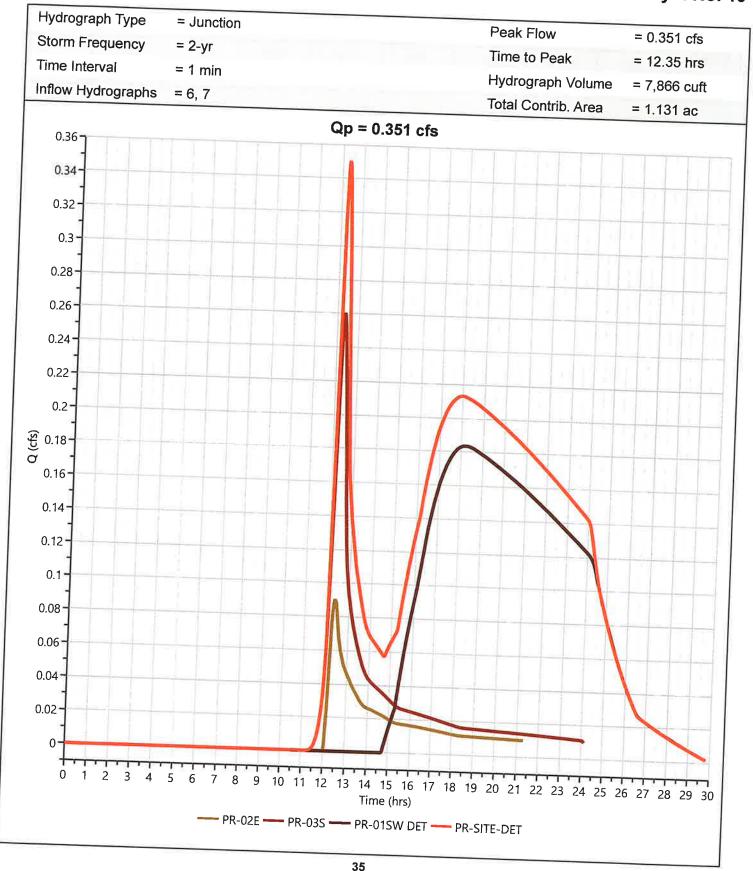
PR-01SW DET

Hyd. No. 9



PR-SITE-DET

Hyd. No. 10



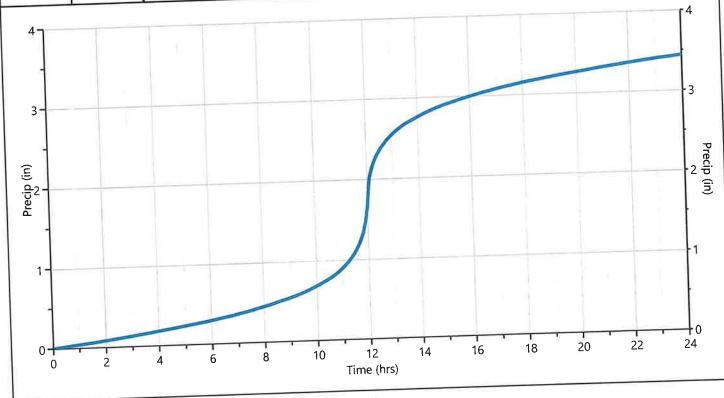
Design Storm Report

Hydrology Studio v 3.0.0.38

Storm Distribution: NOAA-D, 24-hr

				Total Rainfa	l Volume (in)			
Storm Duration		1	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Duration	1-yr	✓ 2-yr	3-y1				7.04	7.90
24 hrs	2.87	3.44	0.00	4.38	5.17	6.24	7.04	7.50

			Increm	ental Rainfa	ll Distribution,	2-yr			
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
		44.70	0.014981	11.97	0.035861	12.15	0.020789	12.33	0.010922
11.60	0.010377	11.78			0.035863	12.17	0.020788	12.35	0.010921
11.62	0.010922	11.80	0.014982	11.98			0.020790	12.37	0.010922
11.63	0.010922	11.82	0.020789	12.00	0.035860	12.18	0.020790		
	0.040000	11.83	0.020790	12.02	0.059837	12.20	0.020788	12.38	0.01092
11.65	0.010922			12.03	0.059841	12.22	0.014981	12.40	0.01092
11.67	0.010922	11.85	0.020789	12.03	4-2	40.00	0.014981	12.42	0.01037
11.68	0.010922	11.87	0.020788	12.05	0.059837	12.23			0.01027
	0.010921	11.88	0.020790	12.07	0.059841	12.25	0.014982	12.43	0.01037
11.70	0.010921			12.08	0.059837	12.27	0.014981	12.45	0.01037
11.72	0.014981	11.90	0.020789			12.28	0.014982	12.47	0.01037
11.73	0.014982	11.92	0.035863	12.10	0.059841	12.28			0.01037
	0.014981	11.93	0.035861	12.12	0.020789	12.30	0.014981	12.48	0.01037
11.75	0.014901		0.005000	12.13	0.020790	12.32	0.010922	12.50	0.01037
11.77	0.014982	11.95	0.035863	12.13	0.02070				



Hydrograph 5-yr Summary

lyd. No.	Hydrograph Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation (ft)	Maximun Storage (cuft)
1	NRCS Runoff	EX-01SW	1.598	12.50	13,048	S ana d a		
2	NRCS Runoff	EX-02E	0.520	12.33	3,507	-		
3	NRCS Runoff	EX-03S	0.166	12.27	1,014	(4514)		
4	Junction	EX-SITE	2.191	12.42	17,569	1, 2, 3		
5	NRCS Runoff	PR-01SW	6.083	12.42	37,542			
6	NRCS Runoff	PR-02E	0.285	12.27	1,661			
7	NRCS Runoff	PR-03S	0.472	12.33	2,624	****		
8	Junction	PR-SITE	6.762	12.42	41,827	5, 6, 7		
9	Pond Route	PR-01SW DET	0.809	14.23	19,134	5	28.70	20,332
10	Junction	PR-SITE-DET	0.921	14.07	23,419	6, 7, 9		

EX-01SW

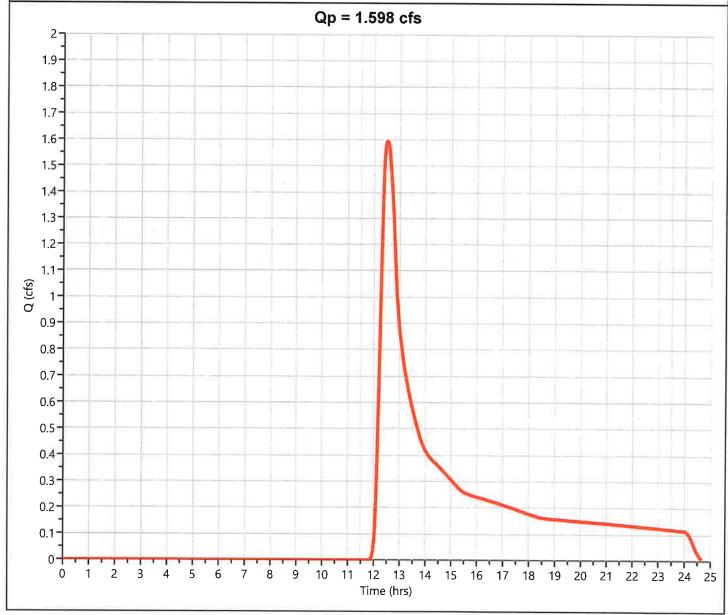
Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.598 cfs
Storm Frequency	= 5-yr	Time to Peak	= 12.50 hrs
Time Interval	= 1 min	Runoff Volume	= 13,048 cuft
Drainage Area	= 5.183 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 31.45 min
Total Rainfall	= 4.38 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 5,183 55,00 Woods

5.183 55.00 Weighted CN Method Employed



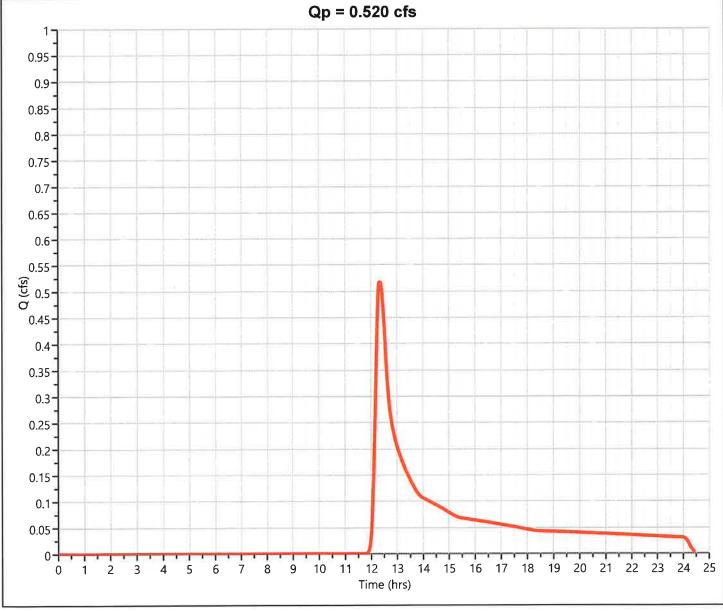
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.520 cfs
Storm Frequency	= 5-yr	Time to Peak	= 12.33 hrs
Time Interval	= 1 min	Runoff Volume	= 3,507 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 4.38 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55,00 Woods

1.389 55.00 Weighted CN Method Employed



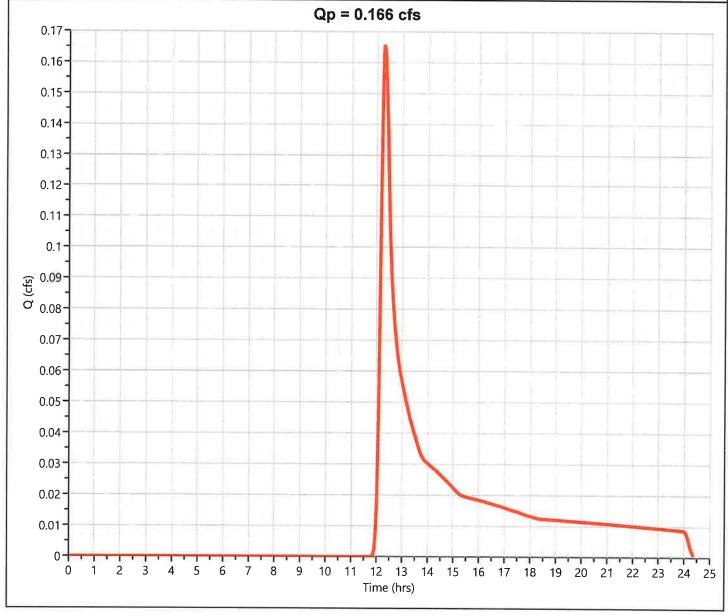
EX-03S Hyd. No. 3

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.166 cfs
Storm Frequency	= 5-yr	Time to Peak	= 12.27 hrs
Time Interval	= 1 min	Runoff Volume	= 1,014 cuft
Drainage Area	= 0.41 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.32 min
Total Rainfall	= 4.38 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 55,00 Woods

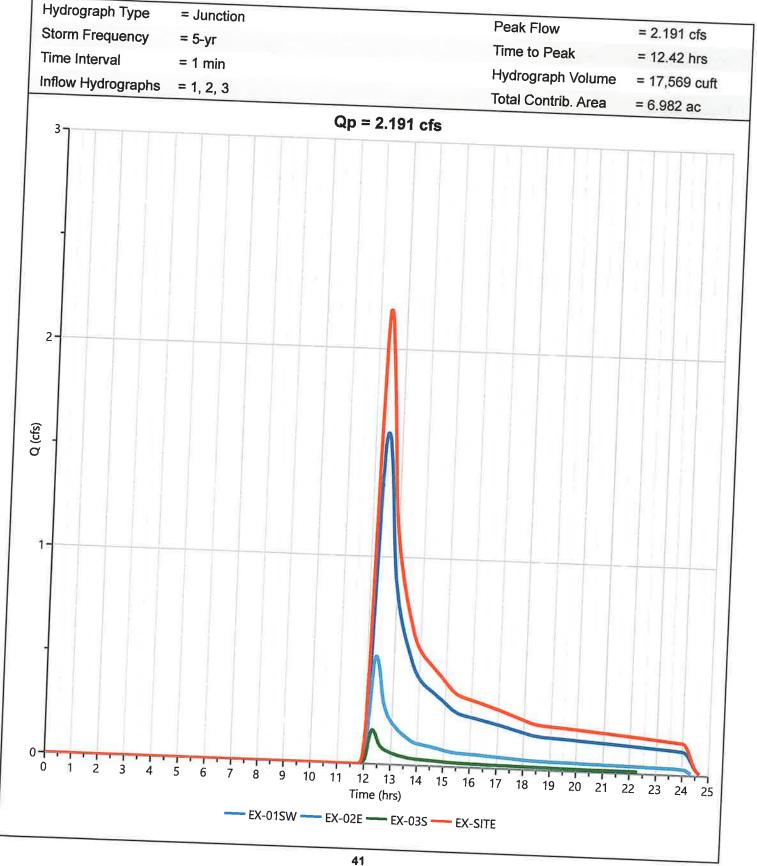
Weighted CN Method Employed 0.41 55.00





EX-SITE

Hyd. No. 4

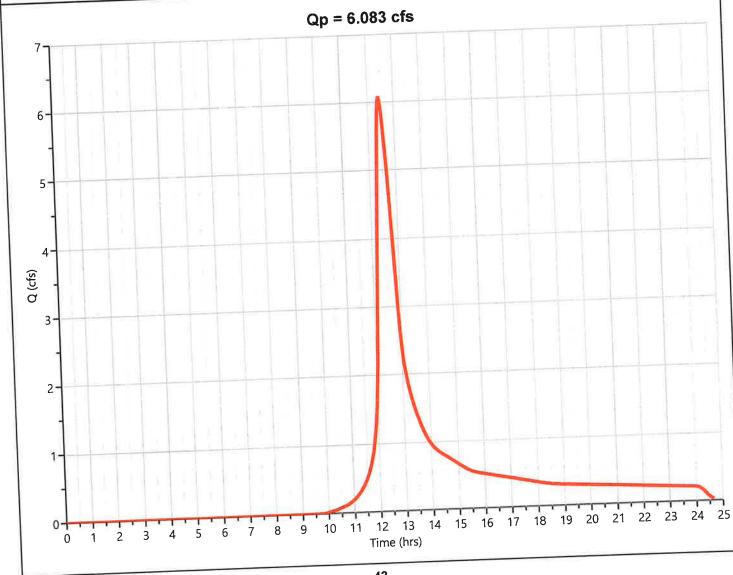


PR-01SW

Hyd. No. 5

		Peak Flow	= 6.083 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.42 hrs
Storm Frequency	= 5-уг	Runoff Volume	= 37,542 cuft
Time Interval	= 1 min	Curve Number	= 72.48*
Drainage Area	= 5.852 ac	Time of Conc. (Tc)	= 34.6 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOAA-D
Total Rainfall	= 4.38 in	Shape Factor	= 484
Storm Duration	= 24 hrs	Onapo i detti	

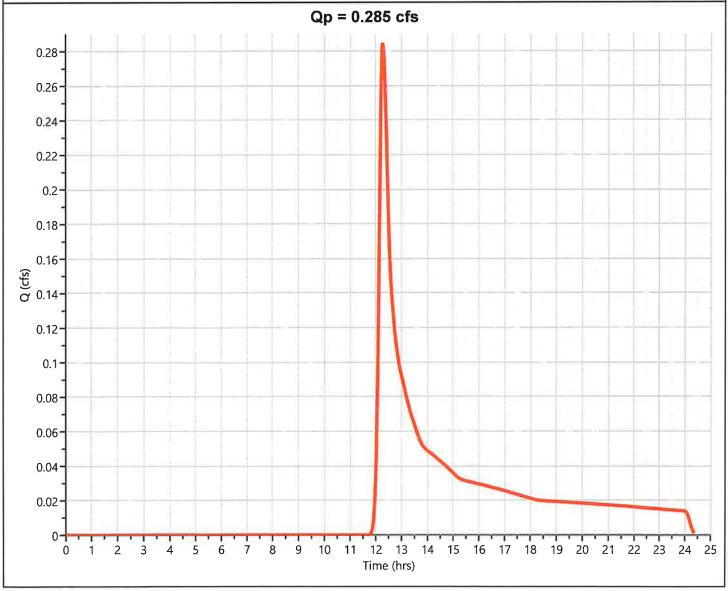
pervious ndscape



PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.285 cfs
Storm Frequency	= 5-yr	Time to Peak	= 12.27 hrs
Time Interval	= 1 min	Runoff Volume	= 1,661 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 4.38 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

AREA (ac)	CN	DESCRIPTION
0.016	61,00	Landscape
0.171	58.00	Conservation
0.44	55,00	Woods
0.627	55.97	Weighted CN Method Employed

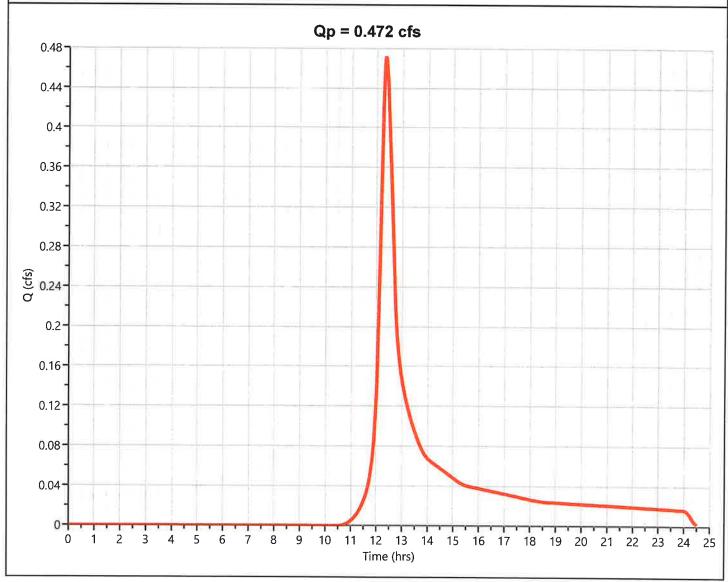


PR-03S

Hyd. No. 7

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.472 cfs
Storm Frequency	= 5-yr	Time to Peak	= 12.33 hrs
Time Interval	= 1 min	Runoff Volume	= 2,624 cuft
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Total Rainfall	= 4.38 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

AREA (ac)	CN	DESCRIPTION
0.12	98.00	Impervious
0.122	61.00	Landscape
0.147	58.00	Conservation
0.115	55.00	Woods
0.504	67.57	Weighted CN Method Emplo



PR-SITE Hyd. No. 8

-lydrograph Type	= Junction		Peak Flow	= 6.762 cfs
Storm Frequency	= 5-yr		Time to Peak	= 12.42 hrs
Time Interval	= 1 min		Hydrograph Volume	= 41,827 cuft
nflow Hydrographs	= 5, 6, 7		Total Contrib. Area	= 6.983 ac
		Qp = 6.762 cfs		
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		Time (hrs)		
	PR-	01SW — PR-02E — PR-03S	PR-SITE	

PR-01SW DET

Hyd. No. 9

Hydrograph Type	= Pond Route	Peak Flow	= 0.809 cfs	
Storm Frequency	= 5-yr	Time to Peak	= 14.23 hrs	
Time Interval	= 1 min	Hydrograph Volume	= 19,134 cuft	
Inflow Hydrograph	= 5 - PR-01SW	Max. Elevation	= 28.70 ft	
Pond Name	= PR-01 DETENTION	Max. Storage	= 20,332 cuft	
Pond Routing by Storage	Indication Method	Center of mas	s detention time = 3,03 h	
	Qp = 0.809 c	fs		
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1				
-1				
0 2	4 6 8 10 12 14 16 Time (hrs)	18 20 22 24	26 28 30	
		ISW DET		



PR-SITE-DET Hyd. No. 10

Hydrograph Type	= Junction		Peak Flow	= 0.921 cfs
Storm Frequency	= 5-yr		Time to Peak	= 14.07 hrs
Time Interval	= 1 min		Hydrograph Volume	= 23,419 cuft
nflow Hydrographs	= 6, 7		Total Contrib. Area	= 1.131 ac
	Qp	= 0.921 cfs		
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0	4 6 8 10 12	14 16 18	20 22 24	26 28

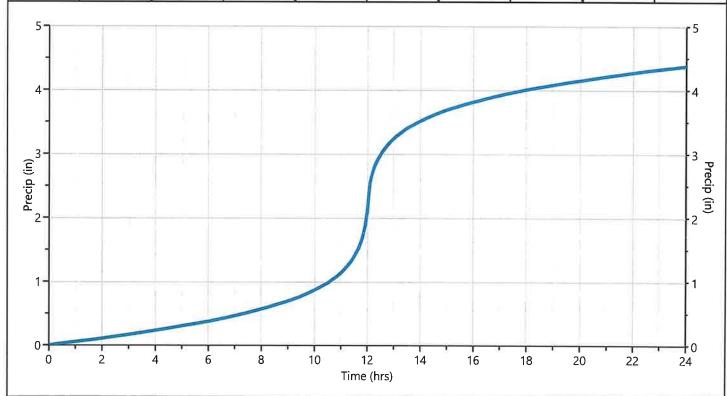
Design Storm Report

Hydrology Studio v 3.0.0.38 10-06-2025

Storm Distribution: NOAA-D, 24-hr

Storm				Total Rainfal	l Volume (in)				
Duration	1-yr	2-уг	3-yr	✓ 5-yr	10-yr	25-yr	50-yr	100-yr	
24 hrs	2.87	3.44	0.00	4.38	5.17	6.24	7.04	7.90	

			Incre	mental Rainf	all Distribution	, 5-yr			
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
11.60	0.013213	11.78	0.019074	11.97	0.045660	12.15	0.026469	12.33	0.013907
11.62	0.013907	11.80	0.019077	11.98	0.045663	12.17	0.026469	12.35	0.013906
11.63	0.013906	11.82	0.026469	12.00	0.045659	12.18	0.026470	12.37	0.013907
11.65	0.013907	11.83	0.026471	12.02	0.076188	12,20	0.026469	12.38	0.013906
11.67	0.013906	11.85	0.026469	12.03	0.076192	12.22	0.019075	12.40	0.013907
11.68	0.013907	11.87	0.026469	12.05	0.076188	12.23	0.019074	12.42	0.013213
11.70	0.013906	11.88	0.026471	12.07	0.076192	12.25	0.019075	12.43	0.013214
11.72	0.019075	11.90	0.026469	12.08	0.076188	12.27	0.019074	12.45	0.013213
11.73	0.019075	11.92	0.045663	12.10	0.076193	12.28	0.019076	12.47	0.013213
11.75	0.019074	11.93	0.045660	12.12	0.026469	12.30	0.019074	12.48	0.013214
11.77	0.019076	11.95	0.045663	12.13	0.026471	12.32	0.013906	12.50	0.013212



Hydrograph 10-yr Summary

File: 20250924PARKERS PLACE Hydrology.hys

No.	Hydrograph Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation	Maximu Storage
1	NRCS Runoff	EX-01SW	2.863	12.43	20,185		(ft)	(cuft)
2	NRCS Runoff	EX-02E	0.942	12.30		-		
3	NRCS Runoff	EX-03S	0.299	12.27	5,426			
4	Junction	EX-SITE	3.958	12.38	1,568			
5	NRCS Runoff	PR-01SW	8.268	12.42	27,178	1, 2, 3		
6	NRCS Runoff	PR-02E	0.495	12.25	50,350			
7	NRCS Runoff	PR-03S	0.670	12.33	2,539			
8	Junction	PR-SITE	9.275	12.40	3,627	TESS.		
9	Pond Route	PR-01SW DET	1.346		56,516	5, 6, 7		
10	Junction	PR-SITE-DET	1.550	13.80	31,680	5	29.31	25,622
			1.550	13.37	37,846	6, 7, 9		
						1	1	

EX-01SW

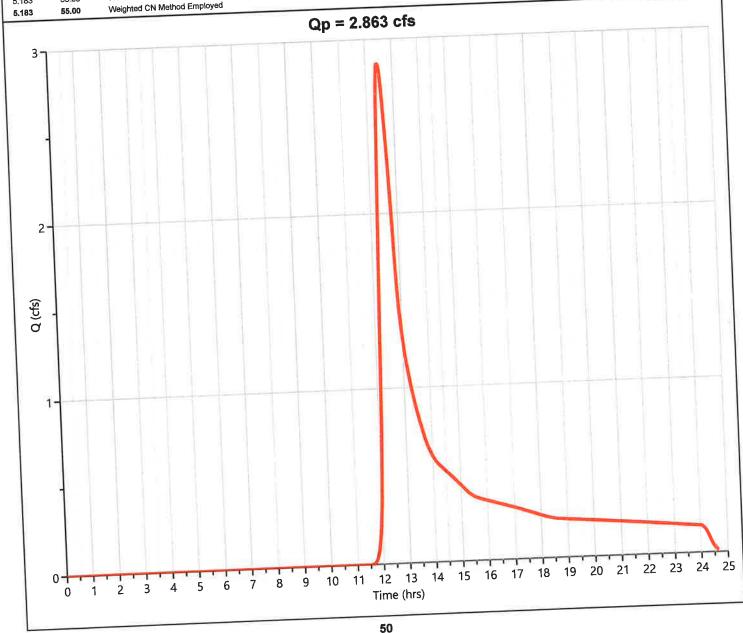
Hyd. No. 1

		Peak Flow	= 2.863 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.43 hrs
Storm Frequency	= 10-yr	Runoff Volume	= 20,185 cuft
Time Interval	= 1 min	Curve Number	= 55.00*
Drainage Area	= 5.183 ac	Time of Conc. (Tc)	= 31.45 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOÁA-D
Total Rainfall	= 5.17 in	Shape Factor	= 484
Storm Duration	= 24 hrs	Ghape i actor	

* Composite CN Worksheet

DESCRIPTION AREA (ac) CN 55.00 Woods

Weighted CN Method Employed



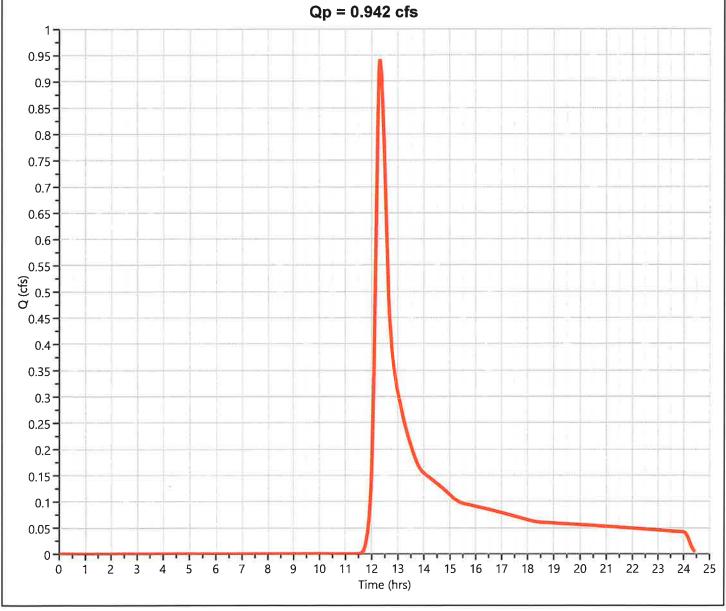
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.942 cfs
Storm Frequency	= 10-yr	Time to Peak	= 12.30 hrs
Time Interval	= 1 min	Runoff Volume	= 5,426 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 5.17 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55,00 Woods

1.389 55.00 Weighted CN Method Employed



EX-03S

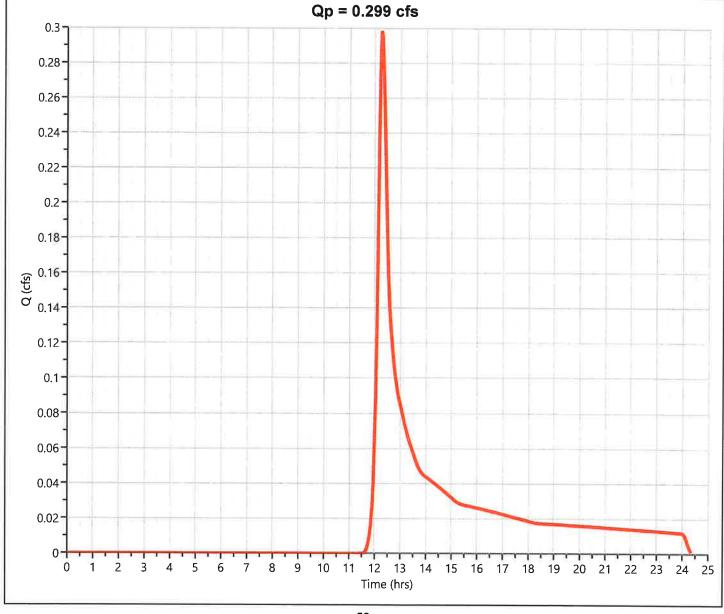
Hyd. No. 3

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.299 cfs
Storm Frequency	= 10-yr	Time to Peak	= 12.27 hrs
Time Interval	= 1 min	Runoff Volume	= 1,568 cuft
Drainage Area	= 0.41 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.32 min
Total Rainfall	= 5.17 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

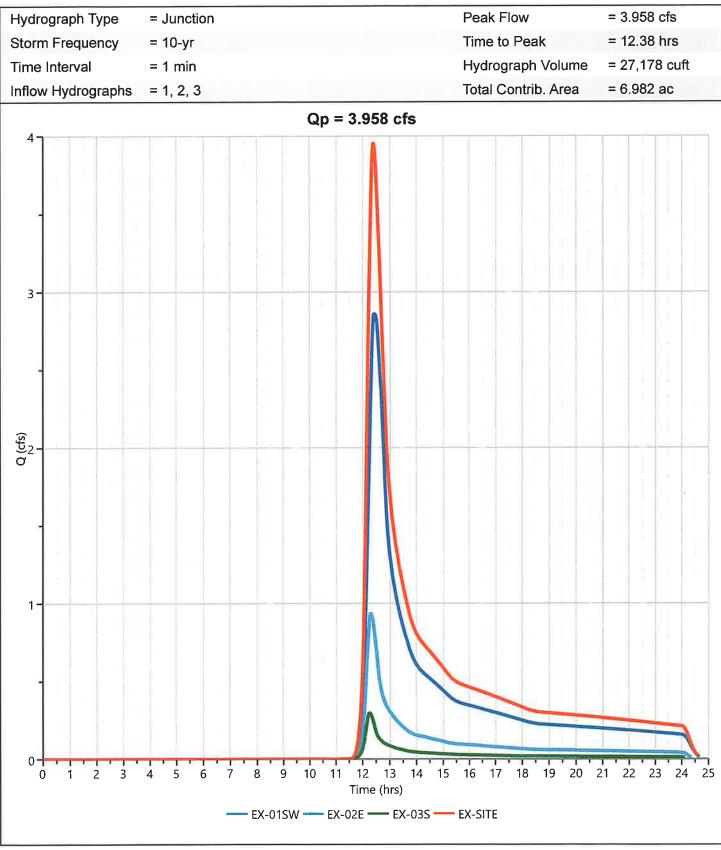
* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.41 55.00 Woods

0.41 55.00 Weighled CN Method Employed



EX-SITE Hyd. No. 4

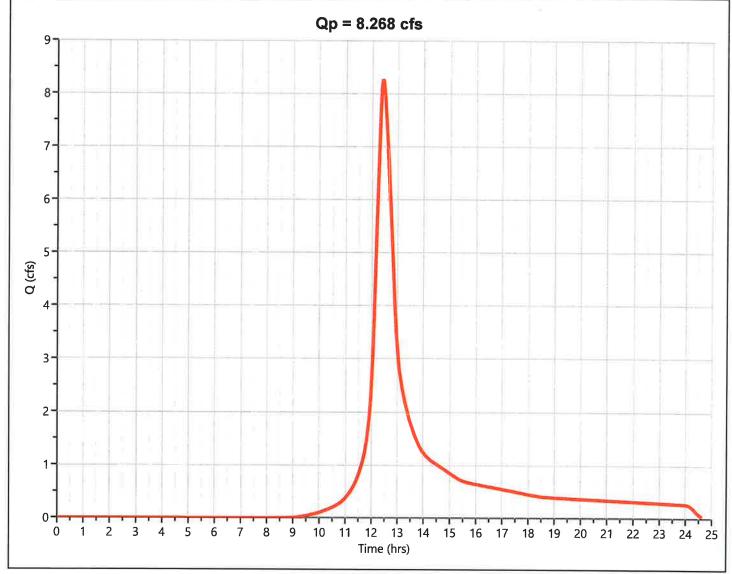


PR-01SW

Hyd. No. 5

Hydrograph Type	= NRCS Runoff	Peak Flow	= 8.268 cfs
Storm Frequency	= 10-yr	Time to Peak	= 12.42 hrs
Time Interval	= 1 min	Runoff Volume	= 50,350 cuft
Drainage Area	= 5.852 ac	Curve Number	= 72.48*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 34.6 min
Total Rainfall	= 5.17 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

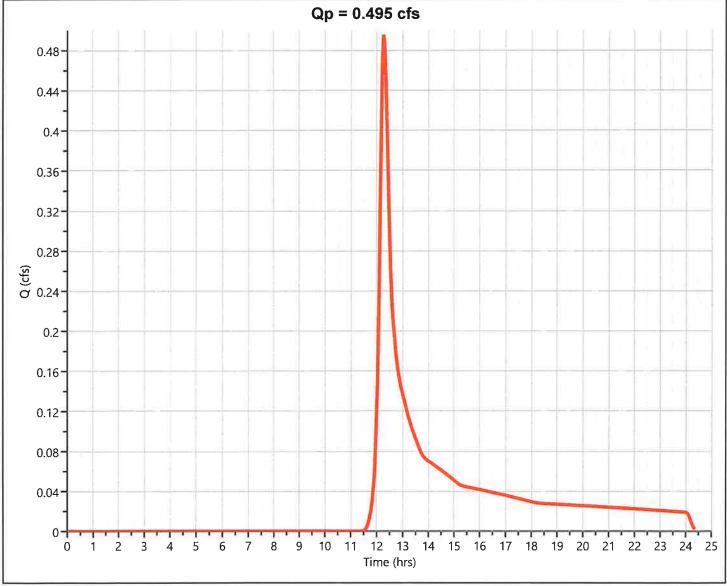
AREA (ac)	CN	DESCRIPTION
2.095	98.00	Impervious
1.395	61.00	Landscape
1.277	58.00	Conservation
1.085	55.00	Woods
5.852	72.48	Weighted CN Method Employed



PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.495 cfs
Storm Frequency	= 10-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 2,539 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 5.17 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

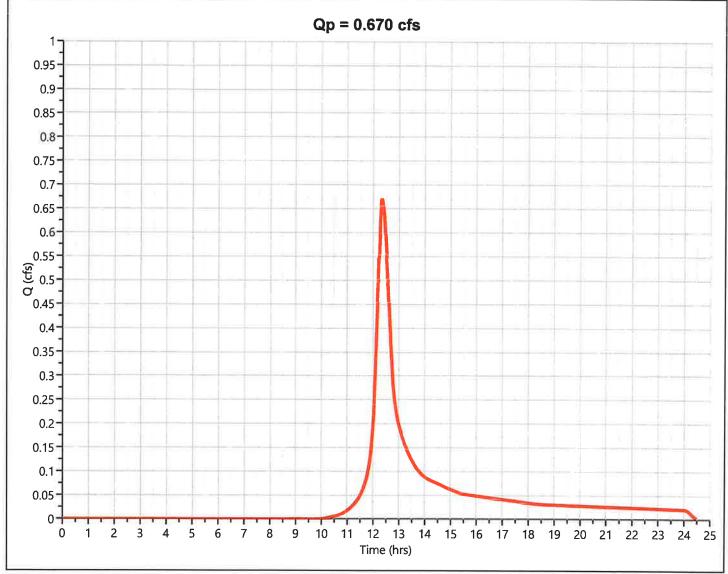
0.627	55.97	Weighted CN Method Employed
0.44	55,00	Woods
0.171	58.00	Conservation
0.016	61.00	Landscape
AREA (ac)	CN	DESCRIPTION



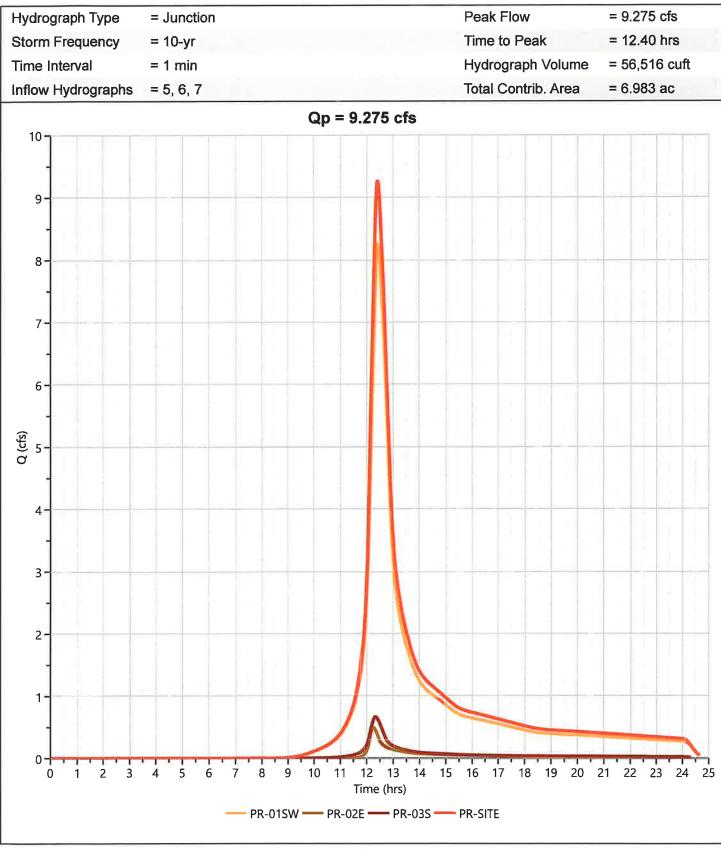
PR-03S Hyd. No. 7

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.670 cfs
		reak rlow	= 0.670 cts
Storm Frequency	= 10-yr	Time to Peak	= 12.33 hrs
Time Interval	= 1 min	Runoff Volume	= 3,627 cuft
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Total Rainfall	= 5.17 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

AREA (ac)	CN	DESCRIPTION
0.12	98.00	Impervious
0.122	61.00	Landscape
0_147	58.00	Conservation
0.115	55,00	Woods
0.504	67.57	Weighted CN Method Employed



PR-SITE Hyd. No. 8



PR-01SW DET

Hydrograph Type	= Pond Route	Peak Flow	= 1.346 cfs	
Storm Frequency	= 10-yr	Time to Peak	= 13.80 hrs	
Time Interval	= 1 min	Hydrograph Volume	= 31,680 cuft	
Inflow Hydrograph	= 5 - PR-01SW	Max. Elevation	= 29.31 ft	
Pond Name = PR-01 DETENTION		Max. Storage	= 25,622 cuft	
Pond Routing by Storage In	dication Method	Center of mass	s detention time = 2.62 h	
	Qp = 1.346 c	fs		
97				
-				
8-				
27-				
7-				
1				
6-				
-				
5-				
(SJD) Q				
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1				
3				
-				
2-				
1-				
1				
0				
4				
-1				
0 2 4	6 8 10 12 14 16 Time (hrs)		26 28 30	
	PR-01SW PR-0	1SW DET		



PR-SITE-DET Hyd. No. 10

Hydrograph Type	= Junction		Peak Flow	= 1.550 cfs				
Storm Frequency	= 10-yr		Time to Peak	= 13.37 hrs = 37,846 cuft				
Time Interval	= 1 min		Hydrograph Volume					
nflow Hydrographs	= 6, 7		Total Contrib. Area	= 1.131 ac				
Qp = 1.550 cfs								
2								
1.9								
1.8								
1.7								
1.6								
1.5		\wedge						
1.4			81 7 3 1 1 1 1					
1.3								
1.2-								
1.1-								
rate the second								
(S) 2 1								
0.9								
0.8		1						
0.7			1					
0.6		N	1					
0.5								
0.4								
0.3								
0.2								
0.1								
0-								
0 1 2 3	4 5 6 7 8 9 10 11	12 13 14 15 16 17 Time (hrs)	18 19 20 21 22 23 24	25 26 27 28 29				
	— PR-02E — PR-	03S — PR-01SW DET —	PR-SITE-DET					

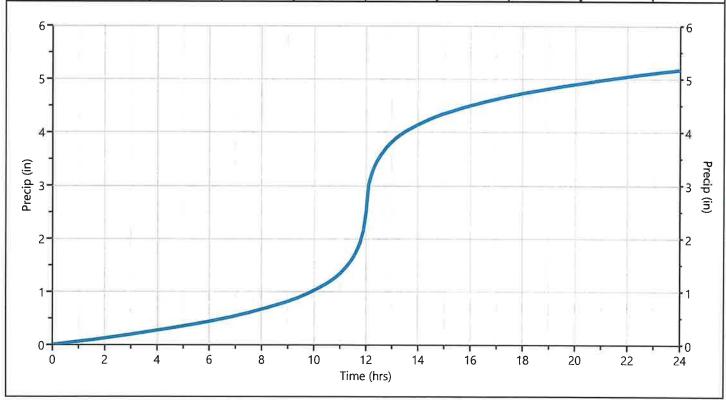
Design Storm Report

Hydrology Studio v 3.0.0.38 10-06-2025

Storm Distribution: NOAA-D, 24-hr

Storm	Total Rainfall Volume (in)								
Duration	1-yr	2-yr	3-yr	5-yr	✓ 10-yr	25-yr	50-уг	100-yr	
24 hrs	2.87	3.44	0.00	4.38	5.17	6.24	7.04	7.90	

	Incremental Rainfall Distribution, 10-yr								
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
11.60	0.015596	11.78	0.022515	11.97	0.053896	12.15	0.031243	12.33	0.016415
11.62	0.016415	11.80	0.022517	11.98	0.053899	12.17	0.031243	12.35	0.016414
11,63	0.016414	11.82	0.031243	12.00	0.053895	12.18	0.031245	12.37	0.016415
11.65	0.016415	11.83	0.031245	12.02	0.089930	12.20	0.031243	12.38	0.016414
11.67	0.016414	11.85	0.031243	12.03	0.089935	12.22	0.022516	12.40	0.016416
11.68	0.016415	11.87	0.031243	12.05	0.089930	12.23	0.022515	12.42	0.015596
11.70	0.016414	11.88	0.031245	12.07	0.089935	12.25	0.022516	12.43	0.015597
11.72	0.022515	11.90	0.031244	12.08	0.089930	12.27	0.022515	12.45	0.015596
11.73	0.022516	11.92	0.053898	12.10	0.089935	12.28	0.022516	12.47	0.015596
11.75	0.022515	11.93	0.053896	12.12	0.031243	12.30	0.022514	12.48	0.015597
11.77	0.022516	11.95	0.053899	12.13	0.031245	12,32	0.016414	12.50	0.015596



Hydrograph 25-yr Summary

File: 20250924PARKERS PLACE Hydrology.hys 10-06-2025

No.	Hydrograph Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	inflow Hyd(s)	Maximum Elevation (ft)	Maximum Storage
1	NRCS Runoff	EX-01SW	4.907	12.40	31,392	****	(15)	(cuft)
2	NRCS Runoff	EX-02E	1.603	12.28	8,438			
3	NRCS Runoff	EX-03S	0.508	12.25	2,439	(State)		
4	Junction	EX-SITE	6.756	12.37	42,269	1, 2, 3		
5	NRCS Runoff	PR-01SW	11.37	12.42	68,776			
6	NRCS Runoff	PR-02E	0.825	12.25	3,910			
7	NRCS Runoff	PR-03S	0.958	12.33	5,100	2000		
8	Junction	PR-SITE	12.88	12.40	77,786			
9	Pond Route	PR-01SW DET	3.636	13.07	49,814	5, 6, 7		
10	Junction	PR-SITE-DET	4.085	13.02	58,823	5 6, 7, 9	29.92	31,457

Hydrograph Report

EX-01SW

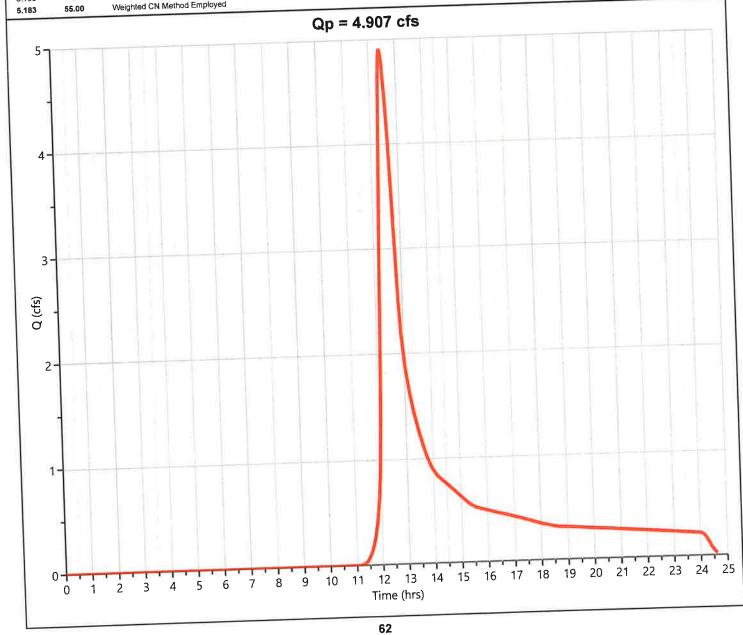
Hyd. No. 1

		Peak Flow	= 4.907 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.40 hrs
Storm Frequency	= 25-yr	Runoff Volume	= 31,392 cuft
Time Interval	= 1 min	Curve Number	= 55.00*
Drainage Area	= 5.183 ac	Time of Conc. (Tc)	= 31.45 min
Tc Method	= TR55 (See Worksheet)		= NOAA-D
Total Rainfall	= 6.24 in	Design Storm	= 484
Storm Duration	= 24 hrs	Shape Factor	- 404

* Composite CN Worksheet

DESCRIPTION AREA (ac) CN Woods 55,00

5.183 Weighted CN Method Employed 55.00



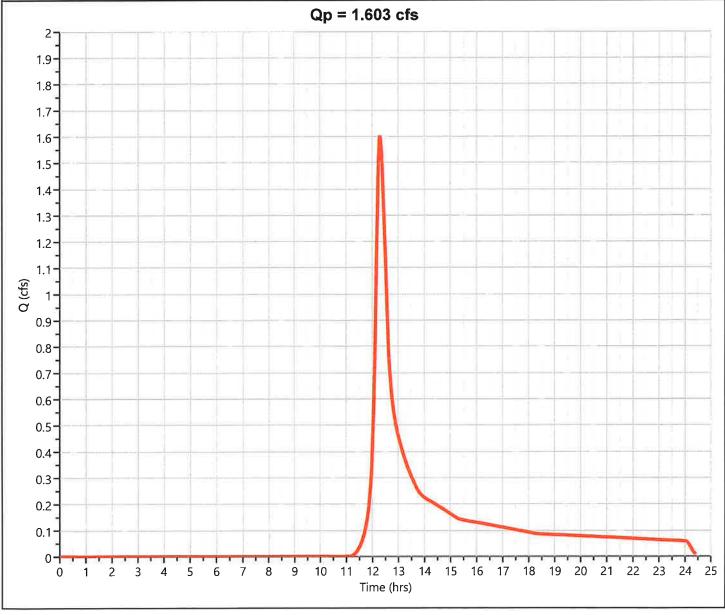
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.603 cfs
Storm Frequency	= 25-yr	Time to Peak	= 12.28 hrs
Time Interval	= 1 min	Runoff Volume	= 8,438 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 6.24 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55,00 Woods

1.389 55.00 Weighted CN Method Employed



EX-03S

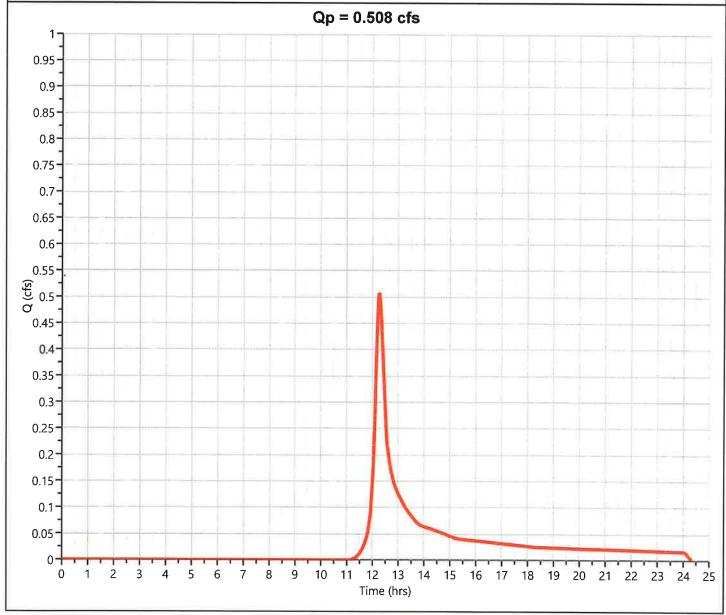
Hyd. No. 3

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.508 cfs
Storm Frequency	= 25-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 2,439 cuft
Drainage Area	= 0.41 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.32 min
Total Rainfall	= 6.24 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

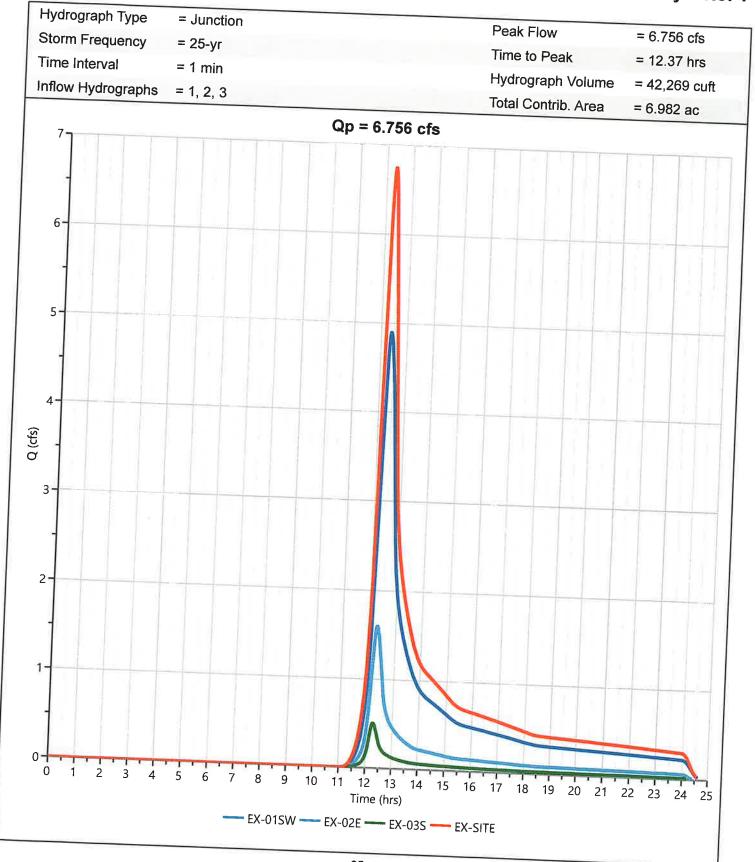
AREA (ac) CN DESCRIPTION 0.41 55,00 Woods

0.41 55.00 Weighted CN Method Employed



EX-SITE

Hyd. No. 4



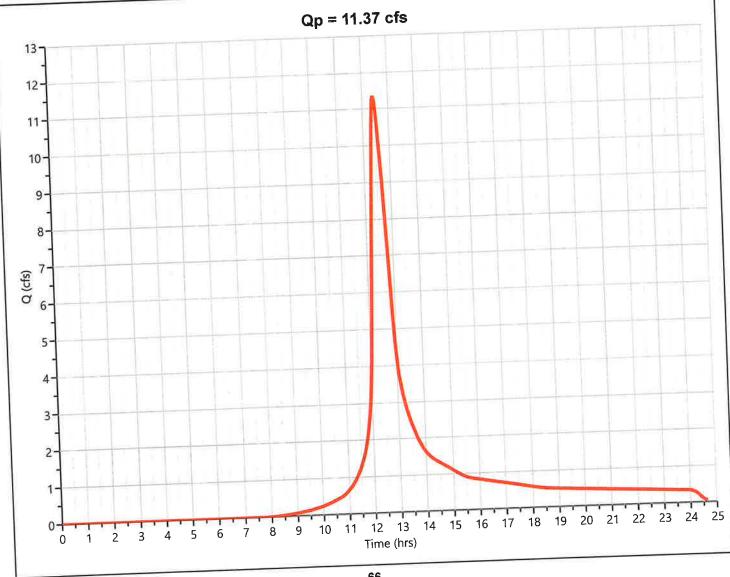
Hydrograph Report

PR-01SW

Hyd. No. 5

		Peak Flow	= 11.37 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.42 hrs
Storm Frequency	= 25-yr	Runoff Volume	= 68,776 cuft
Time Interval	= 1 min	Curve Number	= 72.48*
Drainage Area	= 5.852 ac	Time of Conc. (Tc)	= 34.6 min
Tc Method	= TR55 (See Worksheet)		= NOAA-D
Total Rainfall	= 6.24 in	Design Storm	= 484
Storm Duration	= 24 hrs	Shape Factor	- 101

AREA (ac)	CN	DESCRIPTION
2.095	98.00	Impervious
1 395	61.00	Landscape
1.277	58,00	Conservation
1.085	55,00	Woods
5.852	72.48	Weighted CN Method Employed





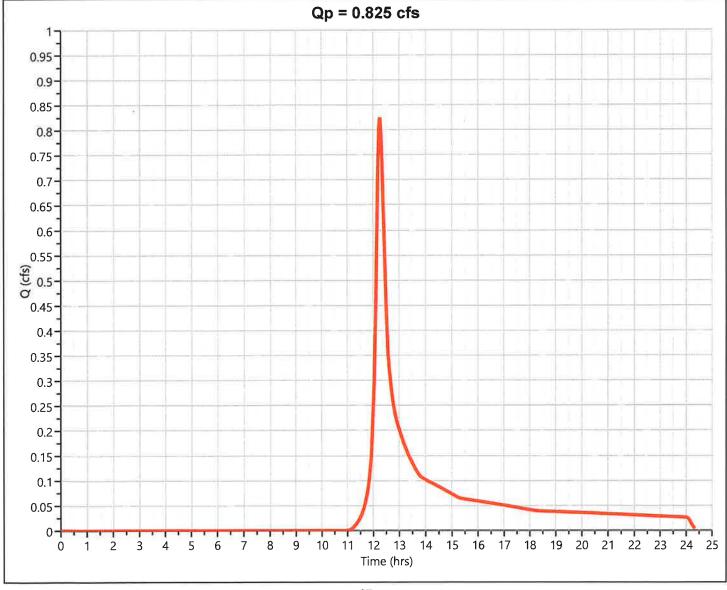
PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.825 cfs
Storm Frequency	= 25-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 3,910 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 6.24 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0,016	61.00	Landscape
0.171	58.00	Conservation
0.44	55.00	Woods

0.627 55.97 Weighted CN Method Employed

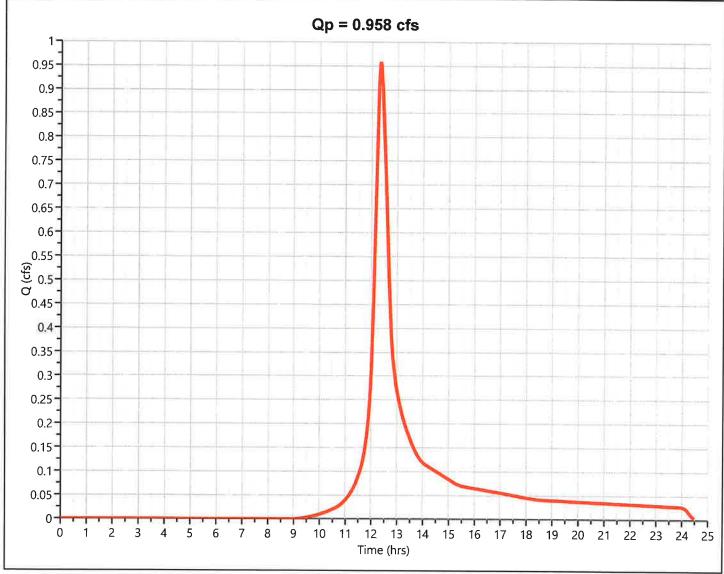


PR-03S

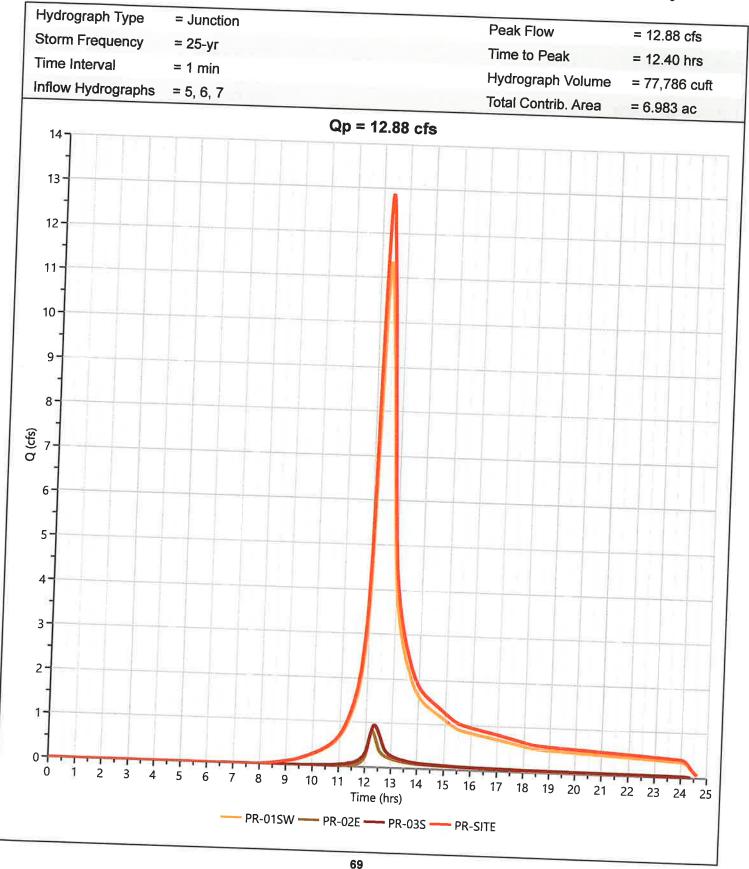
Hyd.	No.	7
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Storm Duration	= 24 hrs	Shape Factor	= 484
Total Rainfall	= 6.24 in	Design Storm	= NOAA-D
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Time Interval	= 1 min	Runoff Volume	= 5,100 cuft
Storm Frequency	= 25-yr	Time to Peak	= 12.33 hrs
Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.958 cfs

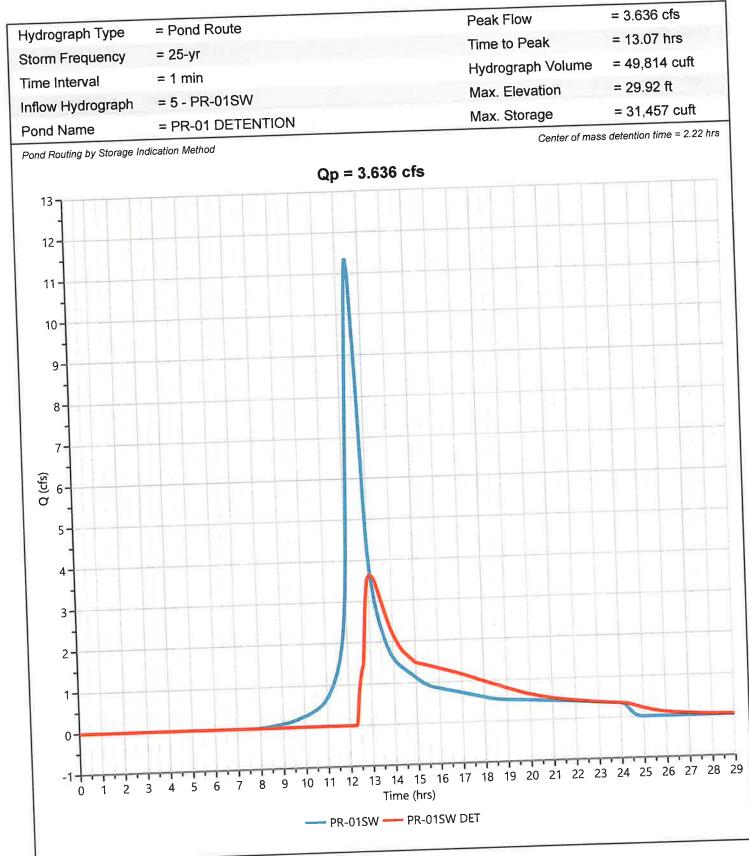
AREA (ac)	CN	DESCRIPTION
0.12	98,00	Impervious
0.122	61.00	Landscape
0.147	58.00	Conservation
0.115	55,00	Woods
0.504	67.57	Weighted CN Method Employed



PR-SITE

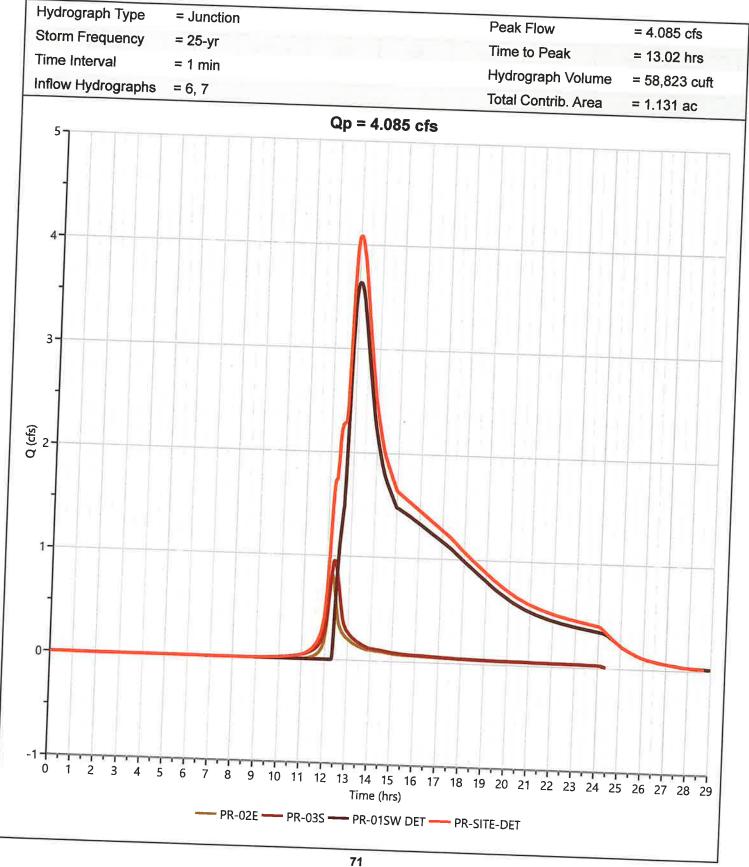


PR-01SW DET





PR-SITE-DET



Design Storm Report

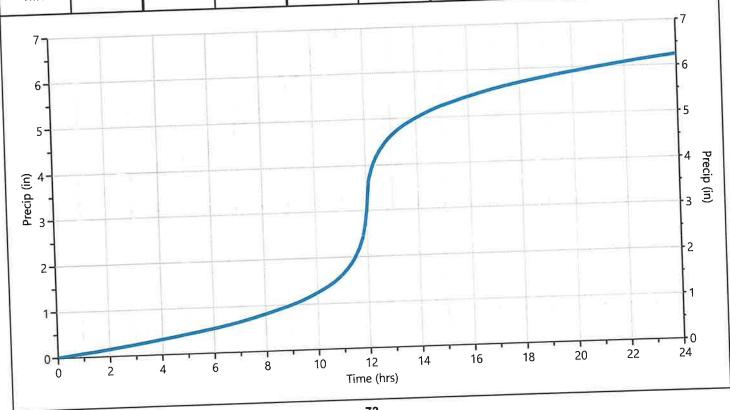
Hydrology Studio v 3.0.0.38

10-06-2025

Storm Distribution: NOAA-D, 24-hr

				Total Rainfal	l Volume (in)			
Storm Ouration		0	3-уг	5-yr	10-yr	✓ 25-yr	50-yr	100-yr
uration	1-yr	2-yr	3-yı			224	7.04	7.90
24 hrs	2,87	3.44	0.00	4.38	5.17	6.24	1.04	7.00

			Incremental Rainfall Distribution, 25-yr							
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	
,		44.70	0.027174	11.97	0.065050	12.15	0.037709	12.33	0.019813	
11.60	0.018824	11.78		11.98	0.065054	12.17	0.037709	12.35	0.019811	
11.62	0.019812	11.80	0.027178			12.18	0.037712	12.37	0.019813	
11.63	0.019812	11.82	0.037709	12,00	0.065049			12.38	0.019811	
11.65	0.019813	11.83	0.037712	12.02	0.108542	12.20	0.037709			
		11.85	0.037709	12.03	0.108548	12.22	0.027175	12.40	0.019814	
11.67	0.019811		0.037709	12.05	0.108542	12.23	0.027174	12.42	0.018823	
11.68	0.019813	11.87			0.108548	12.25	0.027176	12.43	0.018825	
11.70	0.019811	11.88	0.037711	12.07			0.027175	12.45	0.018824	
11.72	0.027174	11.90	0.037710	12.08	0.108542	12.27			0.018824	
	0.027176	11.92	0.065053	12.10	0.108548	12.28	0.027176	12.47		
11.73			0.065050	12.12	0.037709	12.30	0.027174	12.48	0.01882	
11.75	0.027175	11.93			0.037712	12.32	0.019812	12.50	0.018824	
11.77	0.027176	11.95	0.065054	12.13	0.007712					



File: 20250924PARKERS PLACE Hydrology.hys 10-06-2025

Hydrograph 50-yr Summary Hydrology Studio v 3.0.0,38

о. Туре	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation (ft)	Maximum Storage (cuft)
1 NRCS Runoff	EX-01SW	6.603	12.40	40,704			
2 NRCS Runoff	EX-02E	2.154	12.28	10,941	2002		
3 NRCS Runoff	EX-03S	0.681	12.25	3,162	1		
4 Junction	EX-SITE	9.080	12.37	54,807	1, 2, 3		
5 NRCS Runoff	PR-01SW	13.77	12.42	83,150	*****		
6 NRCS Runoff	PR-02E	1.095	12.25	5,043	-		mt
7 NRCS Runoff	PR-03S	1.183	12.33	6,265	344		
8 Junction	PR-SITE	15.67	12.40	94,458	5, 6, 7		own r
9 Pond Route	PR-01SW DET	5.198	12.97	64,010	5	30.34	35,927
10 Junction	PR-SITE-DET	5.816	12.88	75,319	6, 7, 9		

EX-01SW

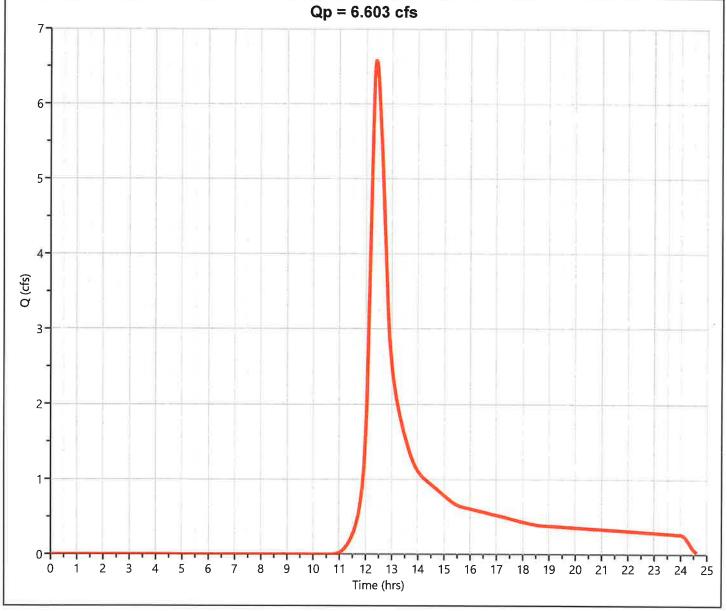
Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 6.603 cfs
Storm Frequency	= 50-yr	Time to Peak	= 12.40 hrs
Time Interval	= 1 min	Runoff Volume	= 40,704 cuft
Drainage Area	= 5.183 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 31.45 min
Total Rainfall	= 7.04 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 5,183 55,00 Woods

5.183 55.00 Weighted CN Method Employed



EX-02E

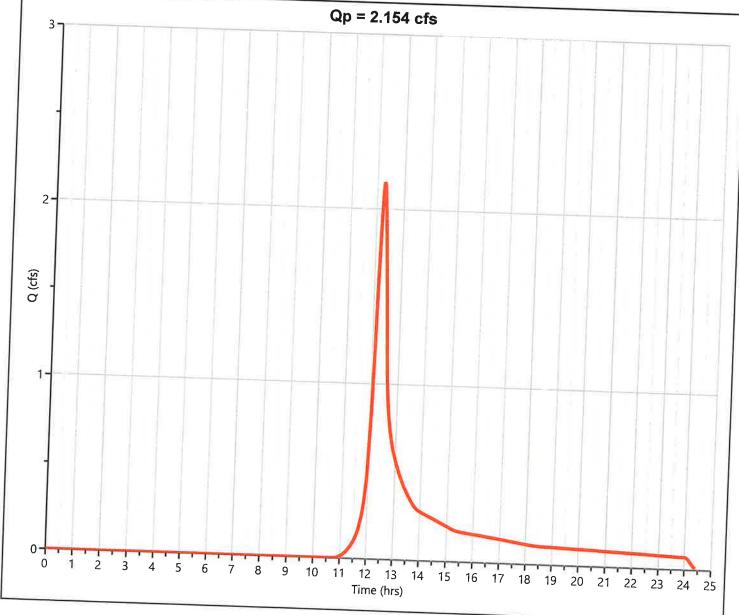
Hyd. No. 2

* Composite CN Workshee	t	Shape Factor	= 484
Storm Duration	= 24 hrs		= NOAA-D
	= 7.04 in	Design Storm	
Total Rainfall		Time of Conc. (Tc)	= 20.61 min
Tc Method	= TR55 (See Worksheet)	Curve Number	= 55.00*
Drainage Area	= 1.389 ac		= 10,941 cuft
Time Interval	= 1 min	Runoff Volume	= 12.28 hrs
	= 50-yr	Time to Peak	
Storm Frequency		Peak Flow	= 2.154 cfs
Hydrograph Type	= NRCS Runoff		

 AREA (ac)
 CN
 DESCRIPTION

 1,389
 55,00
 Woods

 1,389
 55,00
 Weighted CN Method Employed



EX-03S

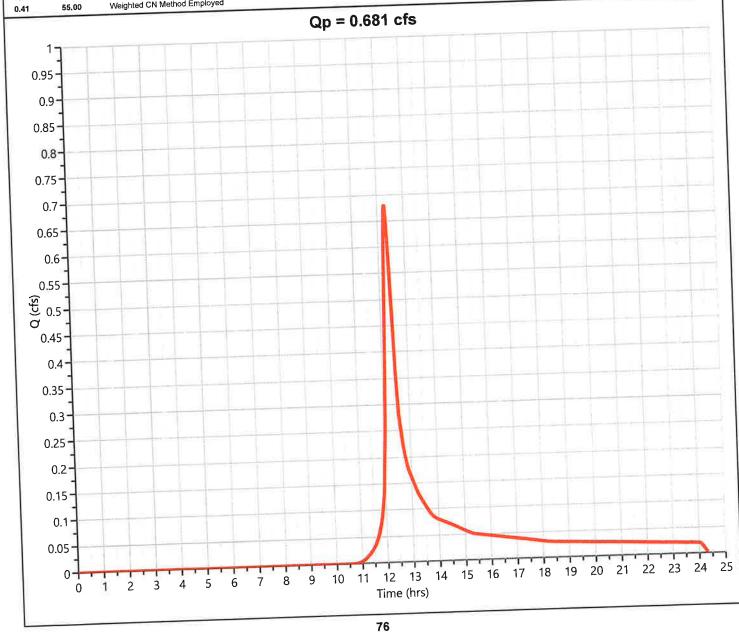
Hyd. No. 3

	<u>.</u>	Peak Flow	= 0.681 cfs
Hydrograph Type	= NRCS Runoff	Time to Peak	= 12.25 hrs
Storm Frequency	= 50-yr	Runoff Volume	= 3,162 cuft
Time Interval	= 1 min	Curve Number	= 55.00*
Drainage Area	= 0.41 ac	Time of Conc. (Tc)	= 18.32 min
Tc Method	= TR55 (See Worksheet)	Design Storm	= NOAA-D
Total Rainfall	= 7.04 in	Shape Factor	= 484
Storm Duration	= 24 hrs	5.1.apo 1 5.5.	

* Composite CN Worksheet

DESCRIPTION AREA (ac) CN Woods

0,41 55,00 Weighted CN Method Employed



EX-SITE Hyd. No. 4

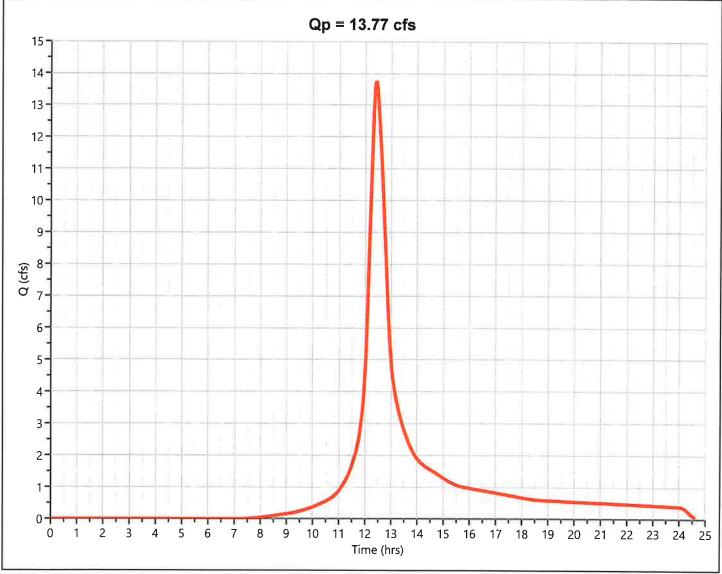
Hydrograph Type	= Junction		Peak Flow	= 9.080 cfs
Storm Frequency	= 50-yr		Time to Peak	= 12.37 hrs
Time Interval	= 1 min		Hydrograph Volume	= 54,807 cuft
inflow Hydrographs	= 1, 2, 3		Total Contrib. Area	= 6.982 ac
		Qp = 9.080 cfs		
10 7				
1				
9				
-				
8-				
7-				
4				
6-				
(S) 5-				
°]				
4-				
1				
3 -				
2				
-				
1-				
0 1 2 3	4 5 6 7 8	9 10 11 12 13 14	15 16 17 18 19 20	21 22 23 24
0 1 2 3	. 5 5 , 6	Time (hrs)		
	EX-0	1SW EX-02E EX-03S	EX-SITE	

PR-01SW

Hyd. No. 5

= NRCS Runoff	Peak Flow	= 13.77 cfs
= 50-yr	Time to Peak	= 12.42 hrs
= 1 min	Runoff Volume	= 83,150 cuft
= 5.852 ac	Curve Number	= 72.48*
= TR55 (See Worksheet)	Time of Conc. (Tc)	= 34.6 min
= 7.04 in	Design Storm	= NOAA-D
= 24 hrs	Shape Factor	= 484
	= 50-yr = 1 min = 5.852 ac = TR55 (See Worksheet) = 7.04 in	= 50-yr Time to Peak = 1 min Runoff Volume = 5.852 ac Curve Number = TR55 (See Worksheet) Time of Conc. (Tc) = 7.04 in Design Storm

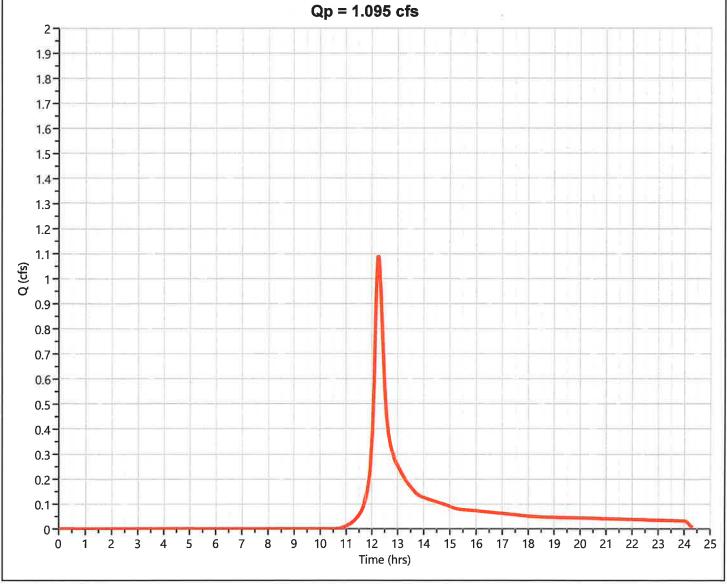
AREA (ac)	CN	DESCRIPTION
2,095	98,00	Impervious
1.395	61,00	Landscape
1,277	58,00	Conservation
1.085	55,00	Woods
5.852	72.48	Weighted CN Method Employed



PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.095 cfs
Storm Frequency	= 50-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 5,043 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 7.04 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

AREA (ac)	CN	DESCRIPTION
0.016	61,00	Landscape
0.171	58.00	Conservation
0.44	55.00	Woods
0.627	55.97	Weighted CN Method Employed



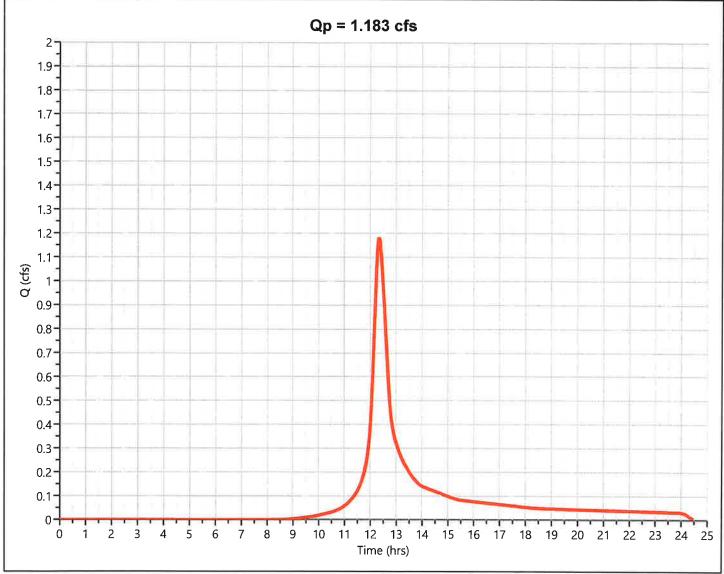
PR-03S Hyd. No. 7

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.183 cfs
Storm Frequency	= 50-yr	Time to Peak	= 12.33 hrs
Time Interval	= 1 min	Runoff Volume	= 6,265 cuft
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Total Rainfall	= 7.04 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

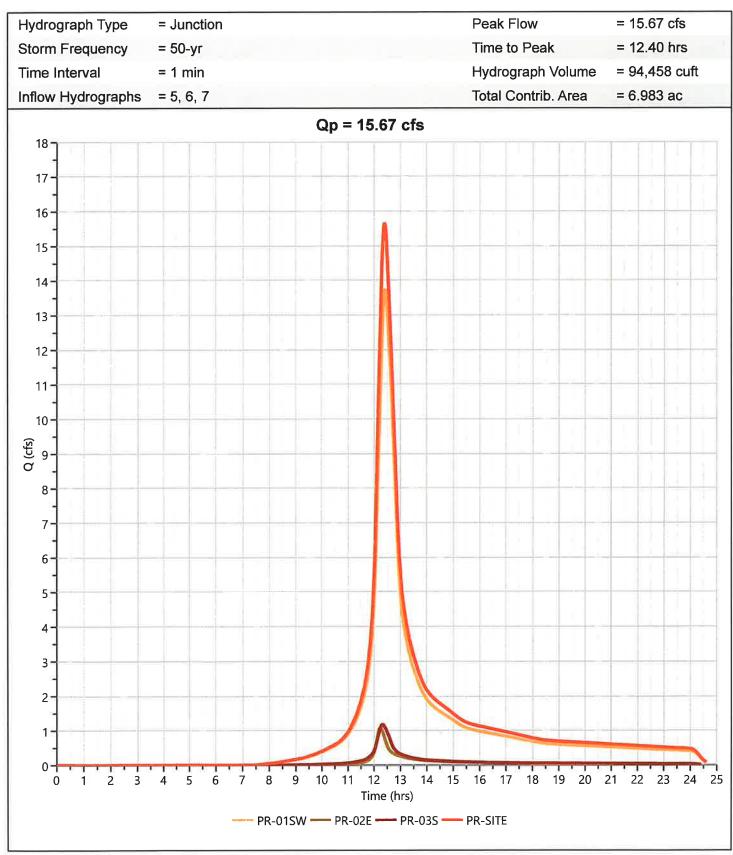
* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0.12	98.00	Impervious
0.122	61.00	Landscape
0.147	58,00	Conservation
0.115	55.00	Woods

0.504 67.57 Weighted CN Method Employed



PR-SITE Hyd. No. 8



PR-01SW DET

Hyd. No. 9

łydrograph Type	= Pond Route	Peak Flow	= 5.198 cfs
Storm Frequency	= 50-yr	Time to Peak	= 12.97 hrs
ime Interval	= 1 min	Hydrograph Volume	= 64,010 cuft
nflow Hydrograph	= 5 - PR-01SW	Max. Elevation	= 30.34 ft
ond Name	= PR-01 DETENTION	Max. Storage	= 35,927 cuft
ond Routing by Storage In	dication Method	Center of mass	s detention time = 1.97
	Qp = 5.198 cfs		
157			
14			
-			
13			
12			
11 -			
10			
9			
-			
8-			
7			
6			
-			
5			
4			
-			
3-			
2			
1			
4			
0			
-1			
0 1 2 3	4 5 6 7 8 9 10 11 12 13 14 15 16 17 Time (hrs)	18 19 20 21 22 23 24	25 26 27 28
		T	



PR-SITE-DET Hyd. No. 10

= Junction	Peak Flow	= 5.816 cfs
= 50-yr	Time to Peak	= 12.88 hrs
= 1 min	Hydrograph Volume	= 75,319 cuft
= 6, 7	Total Contrib. Area	= 1.131 ac
Qp = 5.816 cf	is	
Λ		
5 6 7 8 9 10 11 12 13 14 15 1 Time (hrs)	16 17 18 19 20 21 22 23 2 ²	4 25 26 27 28
	= 50-yr = 1 min = 6, 7 Qp = 5.816 cf	= 50-yr

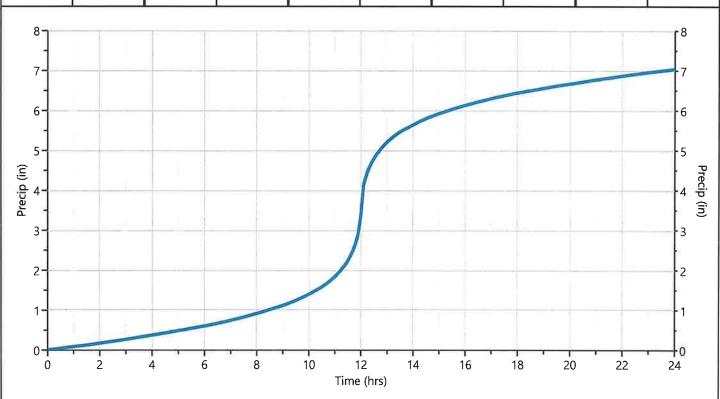
Design Storm Report

Hydrology Studio v 3.0.0.38 10-06-2025

Storm Distribution: NOAA-D, 24-hr

Storm Duration	Total Rainfall Volume (in)								
	1-yr	2-yr	3-yr	5-yr	10-yr	25-уг	✓ 50-yr	100-yr	
24 hrs	2.87	3.44	0.00	4.38	5.17	6.24	7.04	7.90	

	Incremental Rainfall Distribution, 50-yr								
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
11.60	0.021237	11.78	0.030658	11.97	0.073390	12.15	0.042544	12.33	0.022353
11.62	0.022352	11.80	0.030662	11.98	0.073394	12.17	0.042544	12.35	0.022351
11.63	0.022352	11.82	0.042544	12.00	0.073389	12.18	0.042546	12.37	0.022353
11.65	0.022353	11.83	0.042546	12.02	0.122458	12.20	0.042544	12.38	0.022351
11.67	0.022351	11.85	0.042544	12.03	0.122464	12.22	0.030659	12.40	0.022353
11.68	0.022353	11.87	0.042544	12.05	0.122458	12.23	0.030658	12.42	0.021237
11.70	0.022351	11.88	0.042546	12.07	0.122464	12.25	0.030660	12.43	0.021238
11.72	0.030658	11.90	0.042544	12.08	0.122458	12.27	0.030659	12.45	0.021237
11.73	0.030660	11.92	0.073394	12.10	0.122465	12.28	0.030660	12.47	0.021237
11.75	0.030658	11.93	0.073390	12.12	0.042544	12.30	0.030658	12.48	0.021238
11.77	0.030660	11.95	0.073394	12.13	0.042547	12.32	0.022351	12.50	0.021236



Hydrograph 100-yr Summary

	Hydrograph Type	Hydrograph Name	Peak Flow (cfs)	Time to Peak (hrs)	Hydrograph Volume (cuft)	Inflow Hyd(s)	Maximum Elevation (ft)	Maximun Storage (cuft)
1	NRCS Runoff	EX-01SW	8.545	12.40	51,435	****		
2	NRCS Runoff	EX-02E	2.784	12.28	13,826	1000		
3	NRCS Runoff	EX-03S	0.879	12.25	3,996	-		
4	Junction	EX-SITE	11.74	12.37	69,257	1, 2, 3		
5	NRCS Runoff	PR-01SW	16.38	12.42	99,029			
6	NRCS Runoff	PR-02E	1.403	12.25	6,346	1200		
7	NRCS Runoff	PR-03S	1.432	12.33	7,565	1900		
8	Junction	PR-SITE	18.74	12.40	112,940	5, 6, 7		
9	Pond Route	PR-01SW DET	8.316	12.85	79,712	5	30.75	40,314
10	Junction	PR-SITE-DET	9.147	12.83	93,622	6, 7, 9		

EX-01SW

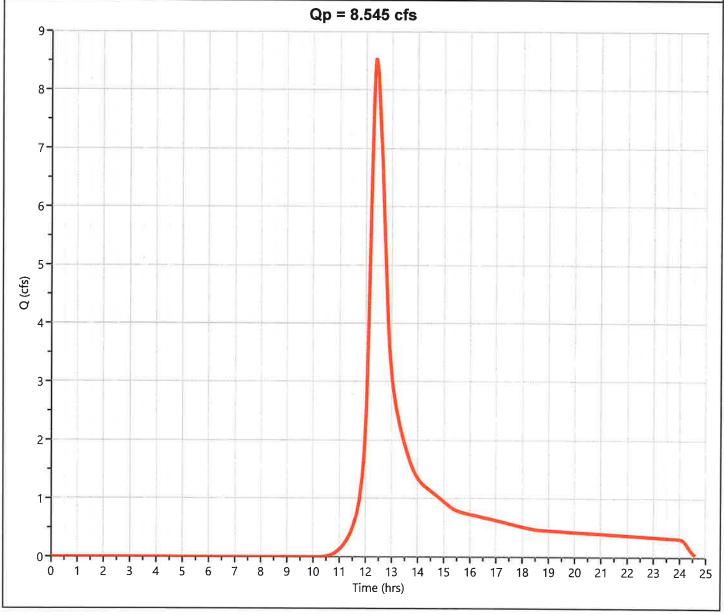
Hyd. No. 1

Hydrograph Type	= NRCS Runoff	Peak Flow	= 8.545 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.40 hrs
Time Interval	= 1 min	Runoff Volume	= 51,435 cuft
Drainage Area	= 5.183 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 31.45 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 5,183 55.00 Woods

5.183 55.00 Weighted CN Method Employed



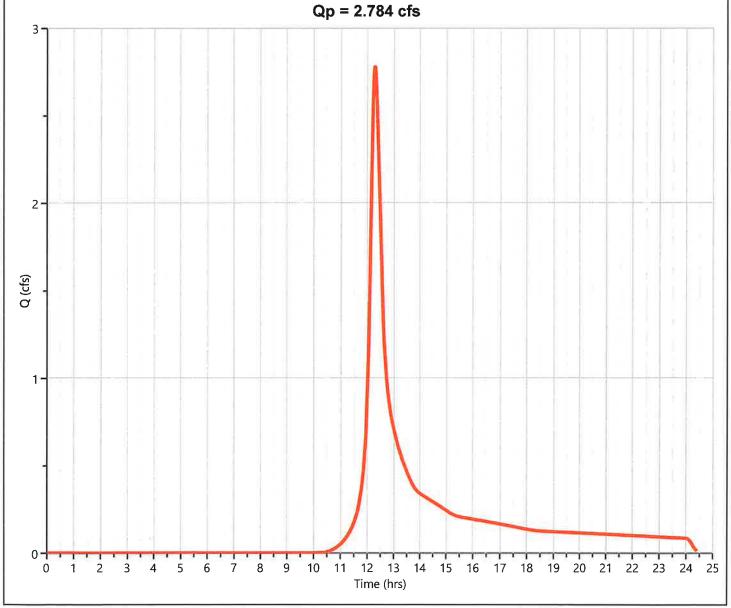
EX-02E Hyd. No. 2

Hydrograph Type	= NRCS Runoff	Peak Flow	= 2.784 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.28 hrs
Time Interval	= 1 min	Runoff Volume	= 13,826 cuft
Drainage Area	= 1.389 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 20.61 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 1,389 55,00 Woods

1.389 55.00 Weighted CN Method Employed



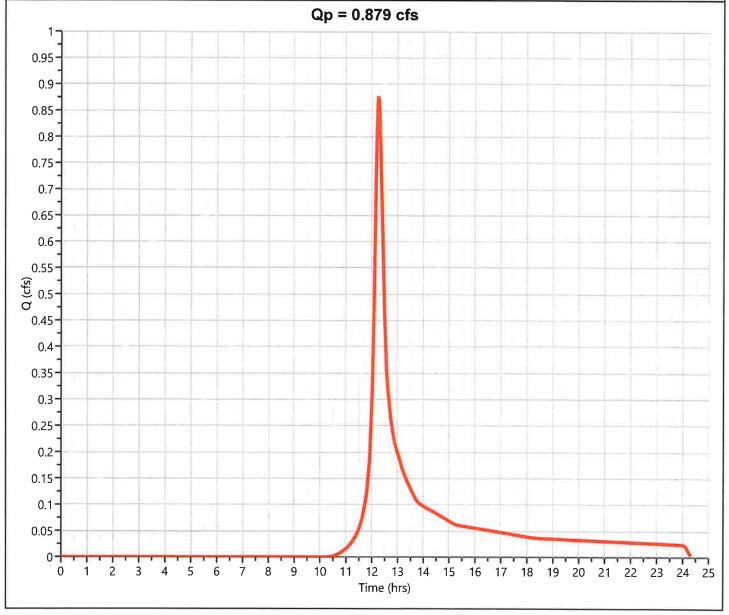
EX-03S Hyd. No. 3

Hydrograph Type	= NRCS Runoff	Peak Flow	= 0.879 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 3,996 cuft
Drainage Area	= 0.41 ac	Curve Number	= 55.00*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.32 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

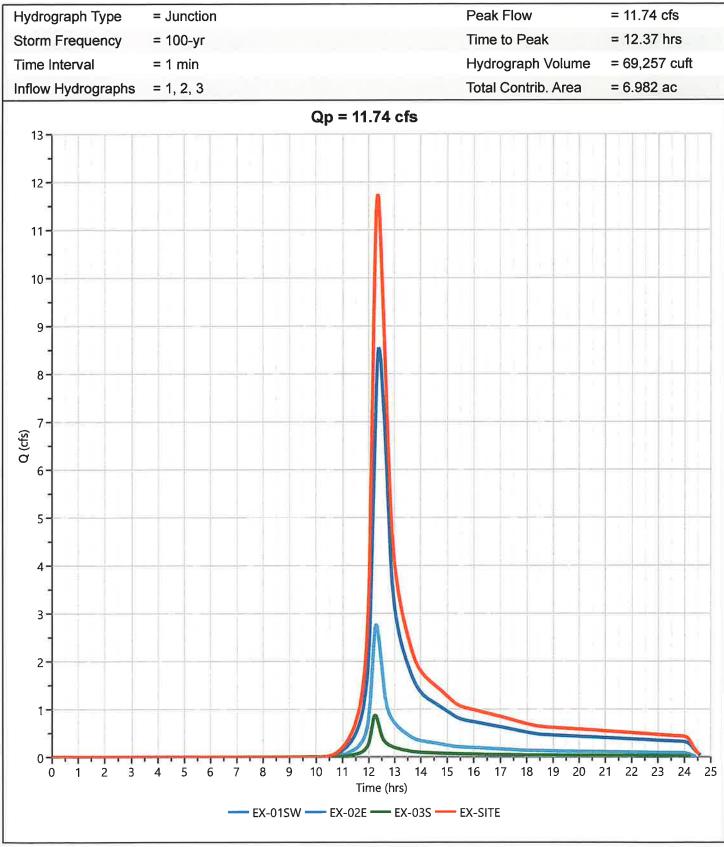
* Composite CN Worksheet

AREA (ac) CN DESCRIPTION 0.41 55.00 Woods

0.41 55.00 Weighted CN Method Employed



EX-SITE Hyd. No. 4



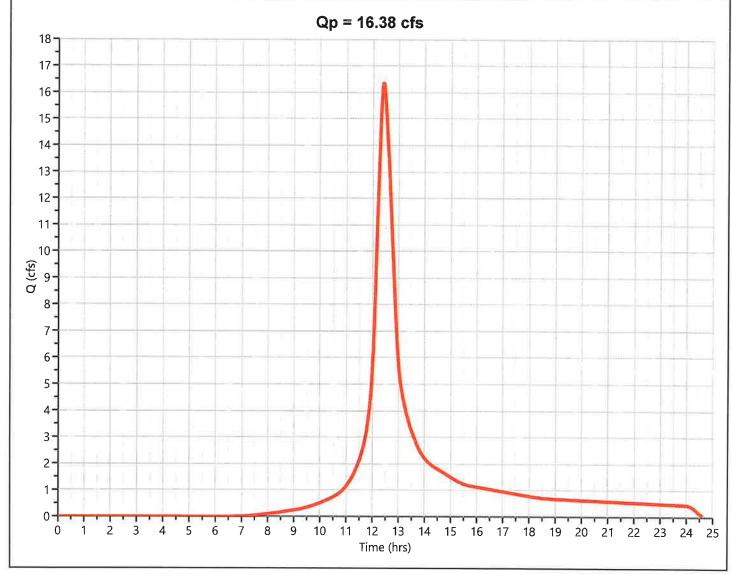
PR-01SW

Hyd. No. 5

Hydrograph Type	= NRCS Runoff	Peak Flow	= 16.38 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.42 hrs
Time Interval	= 1 min	Runoff Volume	= 99,029 cuft
Drainage Area	= 5.852 ac	Curve Number	= 72.48*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 34.6 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
2.095	98.00	Impervious
1.395	61,00	Landscape
1,277	58.00	Conservation
1,085	55.00	Woods
5.852	72.48	Weighted CN Method Employ

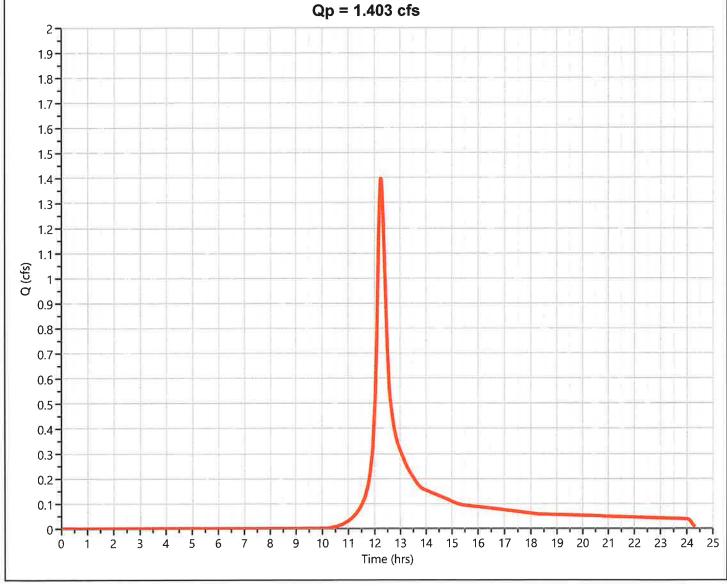


PR-02E Hyd. No. 6

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.403 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.25 hrs
Time Interval	= 1 min	Runoff Volume	= 6,346 cuft
Drainage Area	= 0.627 ac	Curve Number	= 55.97*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 18.27 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0,016	61.00	Landscape
0.171	58.00	Conservation
0.44	55.00	Woods
0.627	55.97	Weighted CN Method Employed

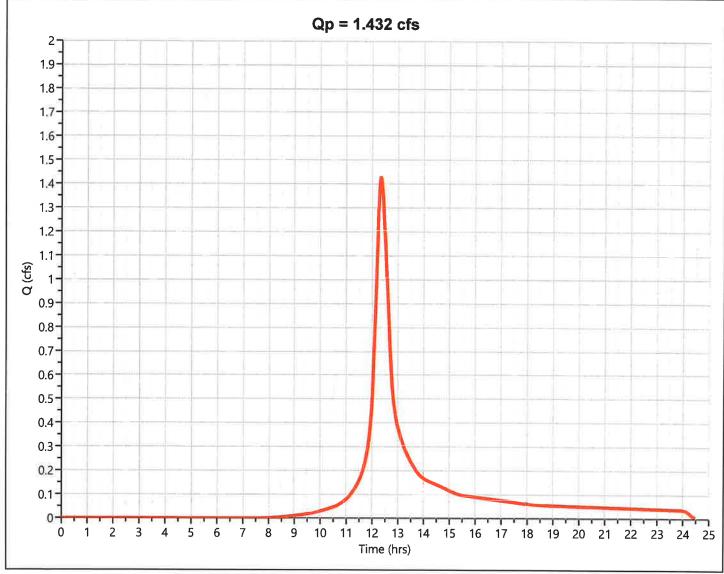


PR-03S Hyd. No. 7

Hydrograph Type	= NRCS Runoff	Peak Flow	= 1.432 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.33 hrs
Time Interval	= 1 min	Runoff Volume	= 7,565 cuft
Drainage Area	= 0.504 ac	Curve Number	= 67.57*
Tc Method	= TR55 (See Worksheet)	Time of Conc. (Tc)	= 26.4 min
Total Rainfall	= 7.90 in	Design Storm	= NOAA-D
Storm Duration	= 24 hrs	Shape Factor	= 484

* Composite CN Worksheet

AREA (ac)	CN	DESCRIPTION
0.12	98.00	Impervious
0.122	61.00	Landscape
0.147	58.00	Conservation
0.115	55.00	Woods
0.504	67.57	Weighted CN Method Employ



PR-SITE Hyd. No. 8

Hydrograph Type	= Junction		Peak Flow	= 18.74 cfs
Storm Frequency	= 100-yr		Time to Peak	= 12.40 hrs
Time Interval	= 1 min		Hydrograph Volume	= 112,940 cuft
Inflow Hydrographs	= 5, 6, 7		Total Contrib. Area = 6.983 ac	
	Qp	= 18.74 cfs		
217				
20				
19				
2-				
18-				
17				
16 -				
15 -		11		1 1 1 1 1
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3				
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1-				
0 1 2 3	4 5 6 7 8 9 10		5 16 17 18 19 20	21 22 23 24
		Time (hrs)		
	PR-01SW —— PI	R-02E — PR-03S —	PR-SITE	

PR-01SW DET Hyd. No. 9

Hydrograph Type	= Pond Route	Peak Flow	= 8.316 cfs
Storm Frequency	= 100-yr	Time to Peak	= 12.85 hrs
Time Interval	= 1 min	Hydrograph Volume	= 79,712 cuft
nflow Hydrograph	= 5 - PR-01SW	Max. Elevation	= 30.75 ft
ond Name	= PR-01 DETENTION	Max. Storage	= 40,314 cuft
Pond Routing by Storage Ir	dication Method		s detention time = 1.79 h
	Qp = 8.316 cfs		
18]			
17-			
16-			
4			
15			
14			
13			
12			
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2			
1-			
0			
-1 -1 			
0 1 2 3	4 5 6 7 8 9 10 11 12 13 14 15 16	17 18 19 20 21 22 23	24 25 26 27 2
	Time (hrs)		

PR-SITE-DET Hyd. No. 10

lydrograph Type	= Junction		Peak Flow	= 9.147 cfs
torm Frequency	= 100-yr		Time to Peak	= 12.83 hrs
ime Interval	= 1 min		Hydrograph Volume	= 93,622 cuft
nflow Hydrographs	= 6, 7		Total Contrib. Area	= 1.131 ac
		Qp = 9.147 cfs		
10 7				
-				
9-				
		1		
8-				
7-				
1				
6-				
4				
5-				
(69)		1 1		
4-				
3				
4				
2-				
1-				
0-				
0 1 2 3	4 5 6 7 8 9 10	11 12 13 14 15 16 1	7 18 19 20 21 22 23	3 24 25 26 27
		Time (hrs)		
	— PR-02E —	PR-03S — PR-01SW DET —	PR-SITE-DET	

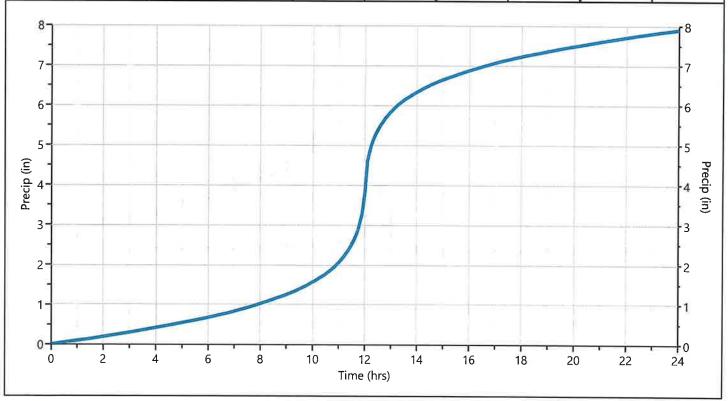
Design Storm Report

Hydrology Studio v 3.0.0.38 10-06-2025

Storm Distribution: NOAA-D, 24-hr

Storm	Total Rainfall Volume (in)								
Duration	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	✓ 100-yr	
24 hrs	2.87	3.44	0.00	4,38	5.17	6.24	7.04	7.90	

			Incren	nental Rainfa	II Distribution,	100-уг			
Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)	Time (hrs)	Precip (in)
11.60	0.023831	11.78	0.034404	11.97	0.082356	12.15	0.047741	12.33	0.025084
11.62	0.025083	11.80	0.034408	11.98	0.082360	12.17	0.047741	12.35	0.025082
11.63	0.025082	11.82	0.047741	12.00	0.082354	12.18	0.047744	12.37	0.025084
11.65	0.025083	11.83	0.047744	12.02	0.137417	12.20	0.047741	12.38	0.025082
11.67	0.025082	11.85	0.047741	12.03	0.137425	12.22	0.034404	12.40	0.025085
11.68	0.025083	11.87	0.047741	12.05	0.137417	12.23	0.034404	12.42	0.023831
11.70	0.025081	11.88	0.047744	12.07	0.137425	12.25	0.034406	12.43	0.023833
11.72	0.034404	11.90	0.047741	12.08	0.137417	12.27	0.034403	12.45	0.023831
11.73	0.034405	11.92	0.082359	12.10	0.137425	12.28	0.034406	12.47	0.023831
11.75	0.034404	11.93	0.082356	12.12	0.047741	12.30	0.034402	12.48	0.023833
11.77	0.034405	11.95	0.082360	12.13	0.047744	12.32	0.025082	12.50	0.023831



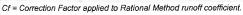
IDF Report

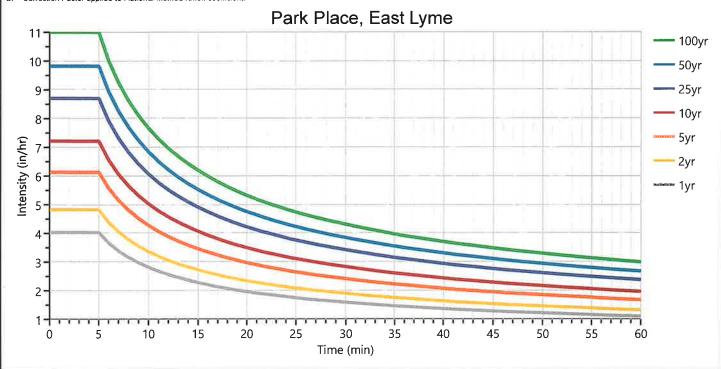
10-06-2025 Hydrology Studio y 3,0,0,38

Equation		Intensity = B / (Tc + D)^E (in/hr)							
Coefficients	1-yr	2-yr	3-yr	5-yr	10-yr	25-уг	50-yr	100-yr	
В	9.3449	11.1753	0.0000	14.2321	16.7547	20.1787	22.8243	25.5746	
D	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	
E	0.5226	0.5225	0.0000	0.5234	0.5239	0.5227	0.5240	0.5242	
_	0.0220								

Minimum Tc = 5 minutes

Тс				Intensity V	alues (in/hr)			
(min)	1-yr	2-yr	3-yr	5-yr	10-yr	25-уг	50-yr	100-yr
Cf	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
5	4.03	4.82	0	6.13	7.21	8.70	9.82	11.00
10	2,81	3.36	0	4.26	5.01	6.06	6.83	7.65
15	2.27	2.71	0	3.45	4.05	4.90	5.52	6.18
20	1.95	2.34	0	2.97	3.49	4.22	4.75	5.32
25	1.74	2.08	0	2.64	3.10	3.75	4.22	4.73
30	1.58	1.89	0	2.40	2.82	3.41	3.84	4.30
35	1.46	1.74	0	2.21	2.60	3.15	3.54	3.97
40	1.36	1.63	0	2.06	2.43	2.93	3.30	3.70
45	1.28	1.53	0	1.94	2.28	2.76	3.10	3.48
50	1.21	1.45	0	1.84	2.16	2.61	2.94	3.29
55	1.15	1.38	0	1.75	2.05	2.48	2.80	3.13
60	1.10	1.32	0	1.67	1.96	2.37	2.67	2.99





Precipitation Report

Hydrology Studio v 3.0.0.38 (Rainfall totals in Inches)

10-06-2025

	Active	1-yr	2-yr	3-уг	5-yr	10-yr	25-yr	50-yr	100
Active		~	~		~	~	~	~	•
SCS Storms	> SCS Dime	nsionless S	Storms					v	
SCS 6hr		1.97	2.36	0	2.99	3.51	4.24	4.77	5.
Type I, 24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.
Type IA, 24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.
Type II, 24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.9
Type II FL, 24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.9
Type III, 24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.
Synthetic Storms	> IDF-Based	Synthetic	Storms		4 4				- ;
1-hr		1.10	1.32	0	1.67	1.96	2.37	2.67	2.9
2-hr		1.53	1.83	0	2.32	2.73	3.30	3.71	4.
3-hr		1.86	2.22	0	2.82	3.31	4.01	4.50	5.0
6-hr		2.59	3.10	0	3.92	4.60	5.58	6.27	7.0
12-hr		3.60	4.31	0	5.46	6.40	7.77	8.71	9.7
24-hr		5.02	6.00	0	7.60	8.90	10.82	12.12	13.
Huff Distribution	> 1st Quartil	e (0 to 6 hr	B):					_ !	
1-hr		1.02	1.22	0	1.55	1.82	2.20	2.48	2.7
2-hr		1.34	1.60	0	2.03	2.39	2.89	3.26	3.6
3-hr		1.55	1.86	0	2.36	2.78	3.35	3.78	4.2
6-hr		1.97	2.36	0	2.99	3.51	4.24	4.77	5.3
Huff Distribution	> 2nd Quarti	ile (>6 to 12	hrs)					, .r. /3	n 1: % -
8-hr		0	0	0	0	0	0	0	0
12-hr		2.45	2.92	0	3.70	4.34	5.23	5.89	6.5
Huff Distribution	> 3rd Quartil	e (>12 to 24	l hrs)					i ve au	4 .
18-hr		0	0	0	0	0	0	0	0
24-hr		2.87	3.44	0	4.38	5.17	6.24	7.04	7.9
Custom Storms	> Custom St	orm Distrib	utions						\$
My Custom Storm 1		0	0	0	0	0	0	0	0
My Custom Storm 2		0	0	0	0	0	0	0	0
My Custom Storm 3		0	0	0	0	0	0	0	0
My Custom Storm 4		0	0	0	0	0	0	0	0
My Custom Storm 5		0	0	0	0	0	0	0	0
My Custom Storm 6		0	0	0	0	0	0	0	0
My Custom Storm 7		0	0	0	0	0	0	0	0
My Custom Storm 8		0	0	0	0	0	0	0	0
My Custom Storm 9		0	0	0	0	0	0	0	0
My Custom Storm 10		0	0	0	0	0	0	0	0

Precipitation Report Cont'd

Rainfall totals in Inches 10-06-2025

	Active 1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-уг
Active	✓	~		~	~	~	~	~
Huff Indiana	> Indianapolis						- E	
30-min	0.79	0.95	0	1.20	1.41	1.70	1.92	2.15
1-hr	1.02	1.22	0	1.55	1.82	2.20	2.48	2.78
2-hr	1.34	1.60	0	2.03	2.39	2.89	3.26	3.65
3-hr	1.55	1.86	0	2.36	2.78	3.35	3.78	4.23
6-hr	1.97	2.36	0	2.99	3.51	4.24	4.77	5.35
12-hr	2.45	2.92	0	3.70	4.34	5.23	5.89	6.59
24-hr	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
Huff Indiana	> Evansville							
30-min	0.79	0.95	0	1.20	1.41	1.70	1.92	2.15
1-hr	1.02	1.22	0	1.55	1.82	2.20	2.48	2.78
2-hr	1.34	1.60	0	2.03	2.39	2.89	3.26	3.65
3-hr	1.55	1.86	0	2.36	2.78	3.35	3.78	4.23
6-hr	1.97	2.36	0	2.99	3.51	4.24	4.77	5.35
12-hr	2.45	2.92	0	3.70	4.34	5.23	5.89	6.59
24-hr	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
Huff Indiana	> Fort Wayne							
30-min	0.79	0.95	0	1.20	1.41	1.70	1.92	2.15
1-hr	1.02	1.22	0	1.55	1.82	2.20	2.48	2.78
2-hr	1.34	1.60	0	2.03	2.39	2.89	3.26	3.65
3-hr	1.55	1.86	0	2.36	2.78	3.35	3.78	4.23
6-hr	1.97	2.36	0	2.99	3.51	4.24	4.77	5.35
12-hr	2.45	2.92	0	3.70	4.34	5.23	5.89	6.59
24-hr	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
Huff Indiana	> South Bend							
30-min	0.79	0.95	0	1.20	1.41	1.70	1.92	2.15
1-hr	1.02	1.22	0	1.55	1.82	2.20	2.48	2.78
2-hr	1.34	1.60	0	2.03	2.39	2.89	3.26	3.65
3-hr	1.55	1.86	0	2.36	2.78	3.35	3.78	4.23
6-hr	1.97	2.36	0	2.99	3.51	4.24	4.77	5.35
12-hr	2.45	2.92	0	3.70	4.34	5.23	5.89	6.59
24-hr	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90

Precipitation Report Cont'd

Rainfall totals in Inches 10-06-2025

	Active	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yı
Activ	е	~	~		~	~	~	~	~
NRCS Storm	s > NRCS D	imensionle	ss Storms						11
NRCS MSE1, 24-I	ır	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCS MSE2, 24-I	ır	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCS MSE3, 24-	or .	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCS MSE4, 24-h	ir ·	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCS MSE5, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCS MSE6, 24-h	r.	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NOAA-A, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NOAA-B, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NOAA-C, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NOAA-D, 24-h	r 🗸 :	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCC-A, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCC-B, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCC-C, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
NRCC-D, 24-h	F	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-1, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-2, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-3, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-4, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-5, 24-h	r ,	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
CA-6, 24-h	r ·	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
FDOT Storm	> Florida É	OT Storms	19 (
FDOT, 1-h	r ·	1.02	1.22	0	1.55	1.82	2.20	2.48	2.78
FDOT, 2-h	r	1.34	1.60	0	2.03	2.39	2.89	3.26	3.65
FDOT, 4-h	г	0	0	0	0	0	0	0	0
FDOT, 8-h	r:	0	, 0	0	0	0	0	0	0
FDOT, 24-h	r	2.87	3.44	0	4.38	5.17	6.24	7.04	7.90
FDOT, 72-h	r	0	0	0	0	0	0	0	0
SFWMD, 72-h	ra	0	. 0	0	0	0	0	0	0
Austin Storm	> Austin Fi	requency S	torms						
Austin Zone 1, 24-h	r :	0	, 0	0	0	0	0	0	0
Austin Zone 2, 24-h	r	0	. 0	0	0	0	0	0	0

STORMWATER TREATMENT CALCULATIONS [PR-01SW]

Compute Water Quality Volume

WQV = Water Quality Volume (acre-feet)

P = 1.3" (90th percentile rainfall event)

R = Volumetric Runoff Coefficient, 0.050 + 0.009(I)

I = Percent Impervious Cover, Impervious Area / Total Area DA =5.852 DCIA = 2.095 acres

DA = Drainage Area (Acres)

DCIA = Directly Connected Impervious Area (Acres)

Determine Percent Impervious Cover (I)

Calculate Volumetric Runoff Coefficient (R)

	C	alculate W	QV		Calculate Sediment Forebay Volume				
	ac-ft		V(req) cf	V(prop) cf	Required	Percent	V(reg) cf	V(prop) cf	
WQV =	0.236	=	10278	14750	Yes	25%	2570	2580	

Compute Runoff Depth

Q = Runoff Depth (in watershed inches) WQV = Water Quality Volume (acre-feet)

DA = Drainage Area (acres)

0.48 watershed inches $Q_{(in)} =$

Determine NCRS Curve Number (CN)

0.48 $Q_{(in)} =$

watershed inches

1.3

TR-55 Figure 2-1

CN =

Determine Initial Abstraction (Ia)

TR-55 Table 4-1

 $I_a =$ 0.247 inches

Determine Unit Peak Discharge (qu)

Time of Concentration (T_c), referenced from Pipe Flow Calculation Worksheet

 $T_c =$ 0.58 hours

 $I_a/P =$ 0.19

TR-55 Exhibit 4-III

 $q_u =$ 350 csm/in

Compute Water Quality Flow

WQF = Water Quality Flow (cfs)

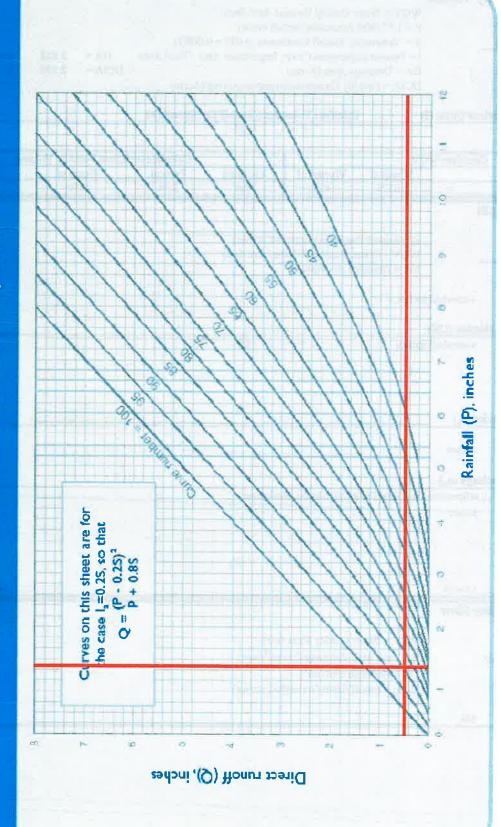
WQF = (qu)(DA)(Q)

qu = unit peak discharge (cfs/mi²/inch)

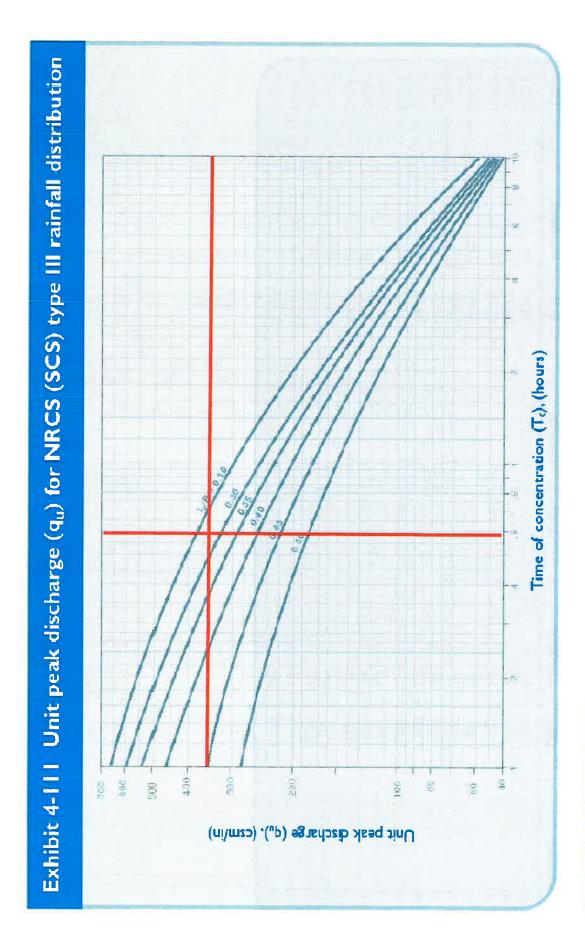
DA = drainage area (mi²)

Q(in) = runoff depth (watershed inches)

WQF = 1.548 cfs



20	Curve I _a number (in)	85
4-1 la values for runoff curve numbers	Curve la number (in)	70 0.857 71 0.817 72 0.740 73 0.740 74 0.667 76 0.632 77 0.597 78 0.564 79 0.532 80 0.500 81 0.439 83 0.410 84 0.381
Table 4-1 la values for	urve mber	55. 1.636 56. 1.571 57. 1.509 58. 1.448 59. 1.390 60. 1.333 61. 1.279 63. 1.175 64. 1.175 65. 1.030 67. 0.985 68. 0.941
F	Curve la number (in)	40 3.000 41 2.878 42 2.762 43 2.651 44 2.545 46 2.444 47 2.255 48 2.167 49 2.000 51 1.922 52 1.846 53 1.774 54 1.704



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STORMWATER TREATMENT CALCULATIONS [PR-03S]

Compute Water Quality Volume

WQV = Water Quality Volume (acre-feet)

P = 1.3" (90th percentile rainfall event)

R = Volumetric Runoff Coefficient, 0.050 + 0.009(I)

I = Percent Impervious Cover, Impervious Area / Total Area DA =0.504 acres

DA = Drainage Area (Acres)

DCIA =

0.120 acres

Determine Percent Impervious Cover (I)

Calculate Volumetric Runoff Coefficient (R)

I =

R =

DCIA = Directly Connected Impervious Area (Acres)

-	C	Calculate W	QV		Calculate Sediment Forebay Volume				
	ac-ft		V(req) cf	V(prop) cf	Required	Percent	V(req) cf	V(prop) cf	
WQV =	0.014	=	629	0	No	0%	0	0	

Compute Runoff Depth

Q = Runoff Depth (in watershed inches)

WQV = Water Quality Volume (acre-feet)

DA = Drainage Area (acres)

 $Q_{(in)} =$

watershed inches

Determine NCRS Curve Number (CN)

0.34

 $Q_{(in)} =$

0.34 watershed inches

in

TR-55 Figure 2-1

CN =

Determine Initial Abstraction (Ia)

TR-55 Table 4-1

0.381 inches $I_a =$

Determine Unit Peak Discharge (q.)

Time of Concentration (Tc), referenced from Pipe Flow Calculation Worksheet

 $T_c =$ 0.44

 $I_a/P =$ 0.29

TR-55 Exhibit 4-III

360

csm/in

hours

Compute Water Quality Flow

WQF = Water Quality Flow (cfs)

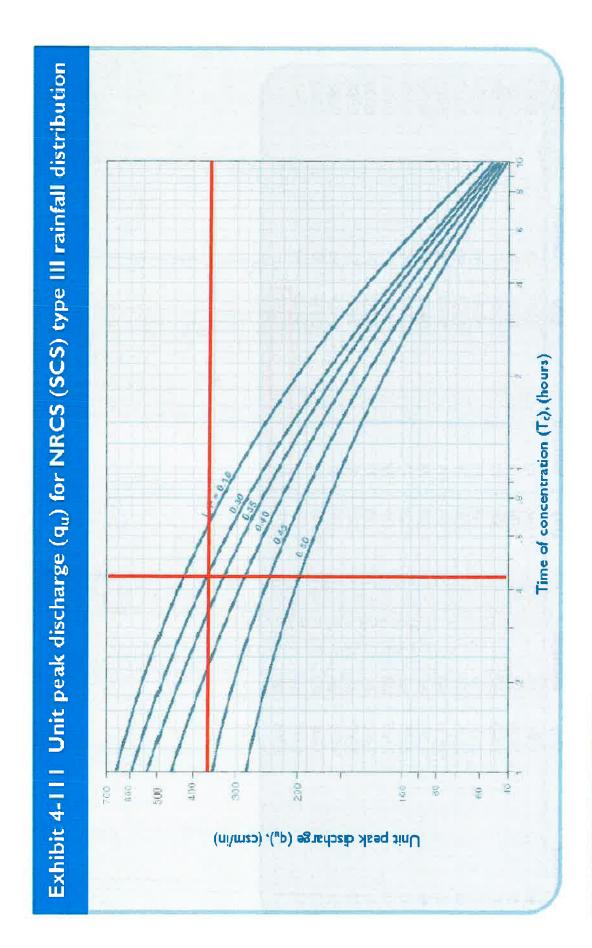
qu = unit peak discharge (cfs/mi²/inch) WQF = (qu)(DA)(Q)

DA = drainage area (mi²)

Q(in) = runoff depth (watershed inches)

WQF = 0.097 cfs

	Curve I _a number (in)	0.0000000000000000000000000000000000000			THE PROPERTY OF STREET		C1 4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (THE REPORT OF THE PROPERTY OF THE PARTY OF T		2 2 2 4 2 4 2 4 2 4 5 4 5 4 5 4 5 4 5 4				
numbers	l _a (in)	0.857 85	+	-	-	H	-	÷	-	-	-	_	-	-	186.0
runoff curve	Curve	70	72	73	74	75	76	77	78	79	80	81	82	83	84
e 4-1 la values for runoff curve numbers	(in)	1636	1509	1.448	0.681	1.333	1.279	1.226	1.175	1.125	1.077	1.030	586.0	0.941	6680
Table 4-1	Curve	55	57	58	59		· · · · · · · · · · · · · · · · · · ·	62	63	64	65	99	67		69
	Curve la number (in)	40 3,000	42 2.762	43 2.651	Contract the Contract of the C	A THE COLUMN TWO IS NOT THE OWNER.	CHARLEST VALLET AND THE SAME	CHARLES AND RIVER BOARD STREET		THE PARTY SHEET AND A SECTION OF	CONTRACTOR CONTRACTOR	511922	*******************	************	STATE OF STATE OF STATE OF STATE



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APPENDIX C

NRCS SOIL DATA NOAA RAINFALL DATA

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Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for State of Connecticut, Eastern Part

PARKERS PLACE



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States
Department of Agriculture and other Federal agencies, State agencies including the
Agricultural Experiment Stations, and local agencies. The Natural Resources
Conservation Service (NRCS) has leadership for the Federal part of the National
Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

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scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

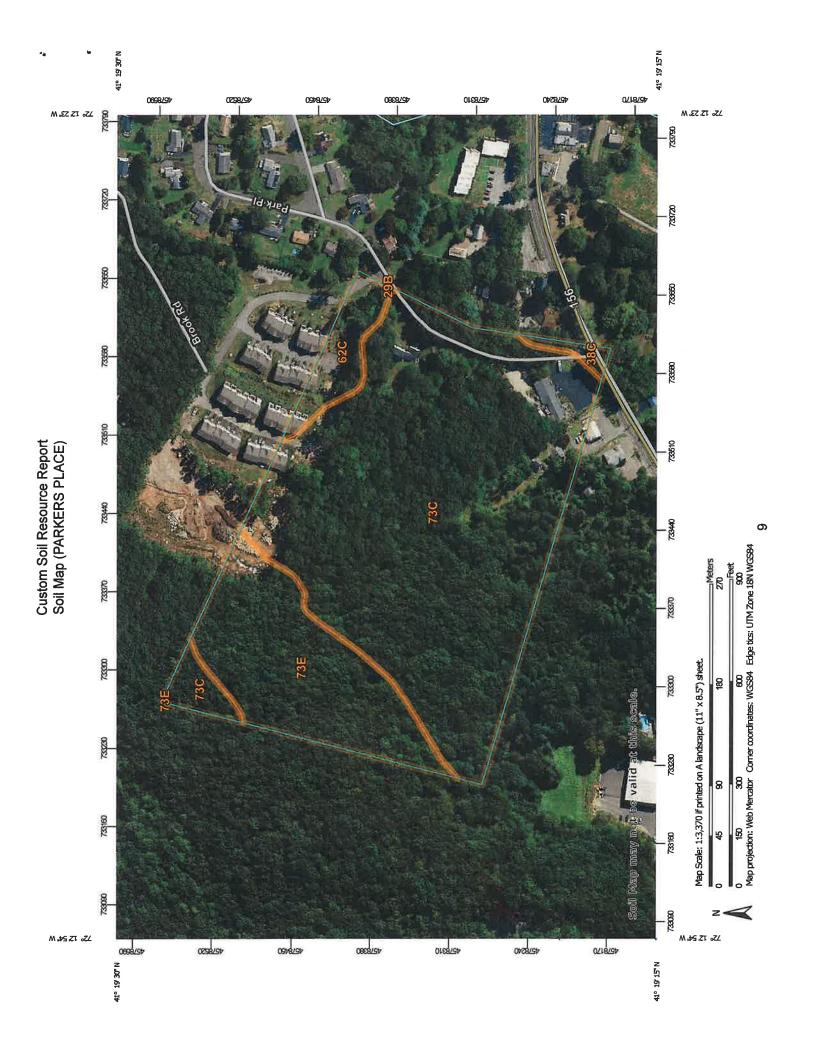
After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Special Line Features Streams and Canals Interstate Highways Aerial Photography Very Stony Spot Major Roads Local Roads Stony Spot US Routes Spoil Area Wet Spot Other Rails Water Features **Fransportation** Background ◁ ŧ Soil Map Unit Polygons Area of Interest (AOI) Miscellaneous Water Soil Map Unit Points Soil Map Unit Lines Closed Depression Marsh or swamp Perennial Water Mine or Quarry Rock Outcrop Special Point Features Gravelly Spot **Borrow Pit Gravel Pit** Lava Flow Clay Spot Area of Interest (AOI) Blowout Landfill

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the

Albers equal-area conic projection, should be used if more

accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut, Eastern Part Survey Area Data: Version 2, Aug 30, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Severely Eroded Spot

Slide or Slip Sodic Spot

Sinkhole

Saline Spot Sandy Spot Date(s) aerial images were photographed: Jun 14, 2022—Oct 6, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend (PARKERS PLACE)

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
29B	Agawam fine sandy loam, 3 to 8 percent slopes	0.0	0.0%
38C	Hinckley loamy sand, 3 to 15 percent slopes	0.2	0.9%
62C	Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony	1.2	4.6%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	19.6	74.1%
73E	Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky	5.4	20.3%
Totals for Area of Interest		26.4	100.0%

Map Unit Descriptions (PARKERS PLACE)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not

Custom Soil Resource Report

mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

State of Connecticut, Eastern Part

29B—Agawam fine sandy loam, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2tyqx

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Agawam and similar soils: 85 percent *Minor components*: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Agawam

Setting

Landform: Outwash terraces

Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Coarse-loamy eolian deposits over sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist and/or phyllite

Typical profile

Ap - 0 to 11 inches: fine sandy loam Bw1 - 11 to 16 inches: fine sandy loam Bw2 - 16 to 26 inches: fine sandy loam 2C1 - 26 to 45 inches: loamy fine sand 2C2 - 45 to 55 inches: loamy fine sand 2C3 - 55 to 65 inches: loamy sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 15 to 35 inches to strongly contrasting textural

stratification

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: B

Ecological site: F145XY008MA - Dry Outwash

Custom Soil Resource Report

Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent Landform: Outwash terraces

Landform position (three-dimensional): Riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

Ninigret

Percent of map unit: 4 percent

Landform: Terraces
Down-slope shape: Linear
Across-slope shape: Concave
Hydric soil rating: No

Hinckley

Percent of map unit: 3 percent

Landform: Eskers

Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

Walpole

Percent of map unit: 3 percent

Landform: Deltas, depressions, outwash terraces, depressions, outwash plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

38C—Hinckley loamy sand, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2svmb

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope,

Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 3 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent

Landform: Kames, outwash plains, outwash terraces, moraines, eskers

Landform position (two-dimensional): Backslope, footslope, shoulder, toeslope,

summit

Landform position (three-dimensional): Side slope, crest, head slope, nose slope,

riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

Windsor

Percent of map unit: 5 percent

Landform: Moraines, eskers, kames, outwash deltas, outwash terraces, outwash

plains, kame terraces

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope,

summit

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Agawam

Percent of map unit: 3 percent

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash

plains, kame terraces

Landform position (two-dimensional): Shoulder, backslope, toeslope, summit,

footslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 2 percent

Landform: Outwash deltas, moraines, outwash plains, kame terraces, outwash

terraces

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

62C—Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony

Map Unit Setting

National map unit symbol: 2wks7

Elevation: 0 to 1,310 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Canton, extremely stony, and similar soils: 50 percent Charlton, extremely stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Canton, Extremely Stony

Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Description of Charlton, Extremely Stony

Setting

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam

C - 27 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Minor Components

Chatfield, extremely stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Leicester, extremely stony

Percent of map unit: 5 percent

Landform: Hills, drainageways, depressions, ground moraines Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

Sutton, extremely stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

73C—Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky

Map Unit Setting

National map unit symbol: 2w698

Elevation: 0 to 1,550 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Charlton, very stony, and similar soils: 50 percent Chatfield, very stony, and similar soils: 30 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Charlton, Very Stony

Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Description of Chatfield, Very Stony

Setting

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 2 inches: fine sandy loam

Bw - 2 to 30 inches: gravelly fine sandy loam

2R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 41 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Minor Components

Rock outcrop

Percent of map unit: 5 percent

Hydric soil rating: No

Hollis, very stony

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

Leicester, very stony

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: Yes

Sutton, very stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

73E—Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky

Map Unit Setting

National map unit symbol: 9|q| Elevation: 0 to 1,200 feet

Mean annual precipitation: 43 to 56 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: Not prime farmland

Map Unit Composition

Charlton and similar soils: 45 percent Chatfield and similar soils: 30 percent

Minor components: 25 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Charlton

Setting

Landform: Hills

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from granite and/or schist

and/or gneiss

Typical profile

Ap - 0 to 4 inches: fine sandy loam Bw1 - 4 to 7 inches: fine sandy loam Bw2 - 7 to 19 inches: fine sandy loam

Bw3 - 19 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

Properties and qualities

Slope: 15 to 45 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Description of Chatfield

Settina

Landform: Ridges, hills Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from granite and/or schist

and/or gneiss

Typical profile

Oa - 0 to 1 inches: highly decomposed plant material

A - 1 to 6 inches: gravelly fine sandy loam
Bw1 - 6 to 15 inches: gravelly fine sandy loam
Bw2 - 15 to 29 inches: gravelly fine sandy loam
2R - 29 to 80 inches: unweathered bedrock

Properties and qualities

Slope: 15 to 45 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Low to high (0.01 to

5.95 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Minor Components

Rock outcrop

Percent of map unit: 10 percent Hydric soil rating: No

Leicester

Percent of map unit: 5 percent Landform: Drainageways, depressions Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: Yes

Sutton, very stony

Percent of map unit: 5 percent Landform: Drainageways, depressions Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

Hollis

Percent of map unit: 3 percent Landform: Ridges, hills Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Unnamed, sandy subsoil

Percent of map unit: 1 percent Hydric soil rating: No

Unnamed, red parent material

Percent of map unit: 1 percent Hydric soil rating: No

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Physical Properties

Soil Physical Properties are measured or inferred from direct observations in the field or laboratory. Examples of soil physical properties include percent clay, organic matter, saturated hydraulic conductivity, available water capacity, and bulk density.

Saturated Hydraulic Conductivity (Ksat), Standard Classes (PARKERS PLACE)

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity is considered in the design of soil drainage systems and septic tank absorption fields.

For each soil layer, this attribute is actually recorded as three separate values in the database. A low value and a high value indicate the range of this attribute for the soil component. A "representative" value indicates the expected value of this attribute for the component. For this soil property, only the representative value is used.

The numeric Ksat values have been grouped according to standard Ksat class limits. The classes are:

Very low: 0.00 to 0.01

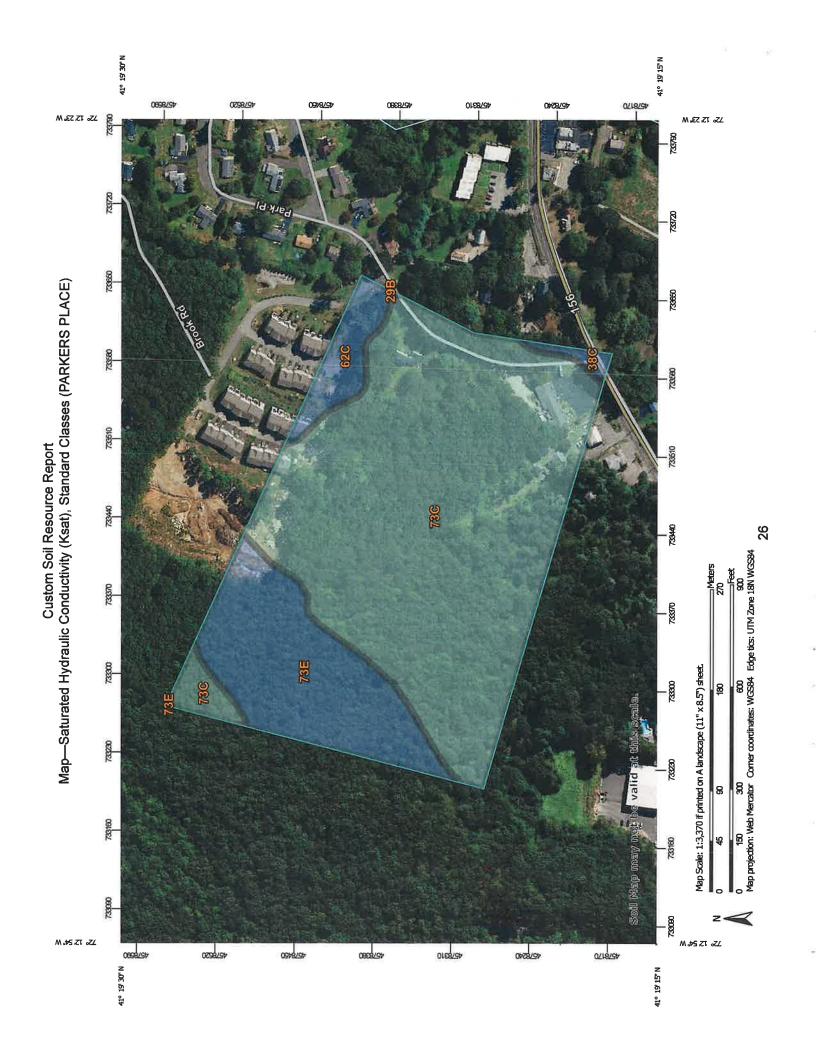
Low: 0.01 to 0.1

Moderately low: 0.1 to 1.0

Moderately high: 1 to 10

High: 10 to 100

Very high: 100 to 705



MAP LEGEND

Not rated or not available Streams and Canals Interstate Highways Aerial Photography Major Roads Local Roads US Routes Rails Water Features Transportation Background ŧ Moderately High (1 - 10) Not rated or not available Moderately Low (0.1 - 1) Moderately Low (0.1 - 1) Not rated or not available Moderately High (1 - 10) Area of Interest (AOI) Moderately Low (0.1 - 1) Moderately High (1 - 10) Very Low (0.0 - 0.01) Very High (100 - 705) Very Low (0.0 - 0.01) Very High (100 - 705) Very Low (0.0 - 0.01) Low (0.01 - 0.1) High (10 - 100) Low (0.01 - 0.1) High (10 - 100) Low (0.01 - 0.1) Soil Rating Polygons Area of Interest (AOI) Soil Rating Lines Soil Rating Points } • B

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut, Eastern Part Survey Area Data: Version 2, Aug 30, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 14, 2022—Oct 6, 2022

Very High (100 - 705)

High (10 - 100)

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Table—Saturated Hydraulic Conductivity (Ksat), Standard Classes (PARKERS PLACE)

Map unit symbol	Map unit name	Rating (micrometers per second)	Acres in AOI	Percent of AOI
29B	Agawam fine sandy loam, 3 to 8 percent slopes	73.4426	0.0	0.0%
38C	Hinckley loamy sand, 3 to 15 percent slopes	100.0000	0.0000 0.2	
62C	Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony	57.2131	1.2	4.6%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	10.0000	19.6	74.1%
73E	Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky	23.0000 5.4		20.3%
Totals for Area of Inte		1,	26.4	100.0%

Rating Options—Saturated Hydraulic Conductivity (Ksat), Standard Classes (PARKERS PLACE)

Units of Measure: micrometers per second
Aggregation Method: Dominant Component
Component Percent Cutoff: None Specified

Tie-break Rule: Fastest Interpret Nulls as Zero: No

Layer Options (Horizon Aggregation Method): Depth Range (Weighted Average)

Top Depth: 12 Bottom Depth: 60

Units of Measure: Inches

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features

include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group (PARKERS PLACE)

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

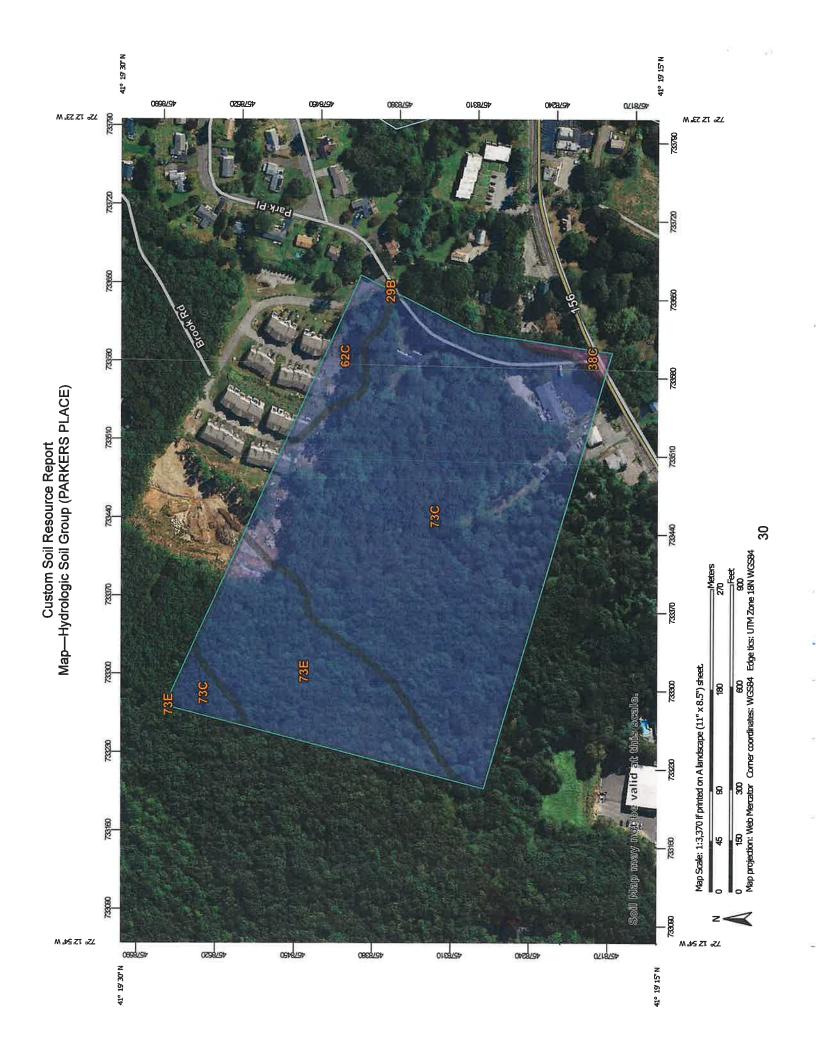
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

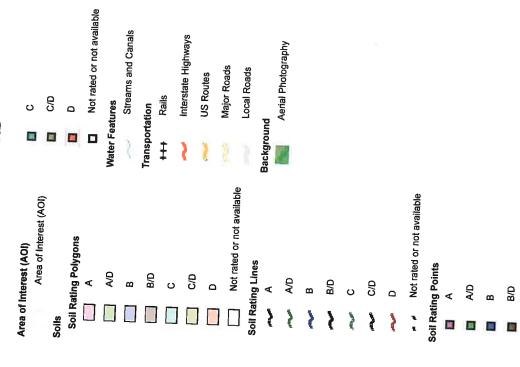
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



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MAP LEGEND



MAP INFORMATION

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Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)

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Soil Survey Area: State of Connecticut, Eastern Part Survey Area Data: Version 2, Aug 30, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 14, 2022—Oct 6, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Table—Hydrologic Soil Group (PARKERS PLACE)

	Map unit name	Rating	Acres in AOI	Percent of AOI
Map unit symbol	triap anno mana		0.0	0.0%
29B	Agawam fine sandy loam, 3 to 8 percent slopes	В		0.9%
38C	Hinckley loamy sand, 3 to 15 percent slopes	A	0.2	
62C	Canton and Chariton fine sandy loams, 3 to 15 percent slopes, extremely stony	В	1.2	74.1%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	19.6	
73E	Charlton-Chatfield complex, 15 to 45 percent slopes, very	В	5.4	20.3%
	rocky		26.4	100.0

Rating Options—Hydrologic Soil Group (PARKERS PLACE)

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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I

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NOAA Atlas 14, Volume 10, Version 3 Location name: Niantic, Connecticut, USA* Latitude: 41.3226°, Longitude: -72.2093° Elevation: 32 ft** source: ESRI Maps
** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite NOAA, National Weather Service, Silver Spring, Maryland

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PF tabular

Duratio	S-based point precipitation frequency estimates with 90% confidence intervals (in inc									nches)1
	1	2	5	10	25	50				
5-min	0.336 (0.259-0.427	0.402 (0.310-0.512)	0.511 (0.393-0.651				0.916	1.03	500	1000
10-min	0.476 (0.367-0.605	(0.310-0.512) 0.570 (0.439-0.725)	0.724		1.00	1.16	1 20	4 40		-
15-min	0.560	0.671 (0.517-0.853)	0.852	1.00	1.21	1.36	1.53	1.46 1) (0.979-2,05	(1.09-2.44)	and described the state of the
30-min	0.790 (0.609-1.00)	0.946	1.20	1.41	(0.897-1.60) 1.70	(0.993-1.84 1.92	(1.08-2.12 2.15) (1.15-2.41) 2.41	-	- Independent account
60-min	1.02 (0.787-1.30)	1.22 (0.941-1.55)	1.55	(1.08-1.81) 1.82	(1.26-2.26) 2.20	(1.40-2.59) 2.48		(1.62-3.40)	1	
2-hr	1.34 (1.04-1.68)	1.60	(1.19-1.98)	(1.39-2.33) 2.39	(1.63-2.91) 2.89	(1.80-3.34) 3.26	(1.97-3.86) 3.65	1	and Barakan and a second	4.01 (2.54-5.8
3-hr	1.55 (1.21-1.94)	1.86	_(1.58-2.57) 2.36	(1.84-3.04) 2.78	(2.16-3.80) 3.35	(2.39-4.36)	(2.61-5.04)	and the Assessment of the Contract of the Cont	4.78 (3.10-6.84)	5.34 (3.39-7.76
6-hr	1.97	2.36	(1.84-2.97) 2.99	(2.15-3.51) 3.51	(2.52-4.39) 4.24	(2.78-5.03) 4.77	4.23 (3.04-5.82)	4.76 (3.22-6.61)	5.55 (3.62-7.91)	6.21 (3.96-8.99
12-hr	(1.56-2.45) 2.45	2.92	(2.35-3.73) 3.70	(2.74-4.40)	(3.21-5.50)	(3.55-6.31)	5.35 (3.86-7.29)	6.02 (4.10-8.28)	7.01 (4.59-9.90)	7.85 (5.02-11.2
24-hr	(1.95-3.02) 2.87	3.44	(2.93-4.58) 4.38	(3.42-5.39)	(3.99-6.73) 6.24	5.89 (4.41-7.71)	6.59 (4.80-8.90)	7.41 (5.08-10.1)	8.62 (5.68-12.1)	9.64 (6.20-13.7
2-day	(2.30-3.51) 3.20	(2.76-4.21) 3.88	(3.51-5.38) 5.00	(4.11-6.36) 5.93	(4.81-7.97)	7.04 (5.31-9.15)	7.90 (5.80-10.6)	8.91 (6.14-12.0)	10.4 (6.90-14.4)	11.7 (7.56-16.4
3-day	(2.60-3.88) 3.47	(3.15-4.71) 4.20	(4.04-6.08) 5.41	(4.76-7.24)	7.21 (5.60-9.14)	8.15 (6.21-10.5)	9.18 (6.81-12.3)	10.4 (7.22-13.9)	12.3 (8.20-16.9)	14.0 (9.06-19.4)
	(2.83-4.18) 3.72	(3.42-5.07)	(4.39-6.54)	6.41 (5.17-7.78)	7.78 (6.08-9.82)	8.80 (6.74-11.3)	9.90 (7.38-13.2)	11.2 (7.81-15.0)	13.3 (8.87-18.2)	15.1 (9.81-20.9)
4-day	(3.05-4.47) 4.44		5.75 (4.68-6.93)	6.79 (5.50-8.22)	8.22 (6.45-10.3)	9.29 (7.13-11.9)	10.4 (7.79-13.8)	11.8	14.0	15.8
	/n nn - 1	(4.34-6.29)	6.62 (5.43-7.92)	7.74 (6.31-9.30)	9.28 (7.32-11.6)	10.4 (8.05-13.2)	11.7 (8.73-15.2)	13.1	15.3	(10.3-21.8) 17.2
	(4.00 - 4-1			8.58 (7.03-10.3)	10.2	11.4	12.7 (9.48-16.4)	14.1	16.3	18.1
	(6.10-8.58)		9.72 (8.10-11.5)	11.0 (9.08-13.0)	12.7	14.0	15.4	16.8	18.8	20.3
			11.6 9.74-13.7)	12.9 (10.8-15.3)	14.8	16.1	17.5	18.9	20.7	(13.4-27.4) 22.1
			14.0 11.8-16.4) (15.4 (12.9-18.1)	17.3	18.8	20.3	21.6	23.2	14.6-29.5) 24.4
O-day	13.2 (11.2-15,3)	14.2 12.1-16.5) (1	16.0	17.5 14.7-20.4) (19.5	21.1	22.6	23.9	15.9-30.4) (° 25.4	16.1-32.4) 26.4

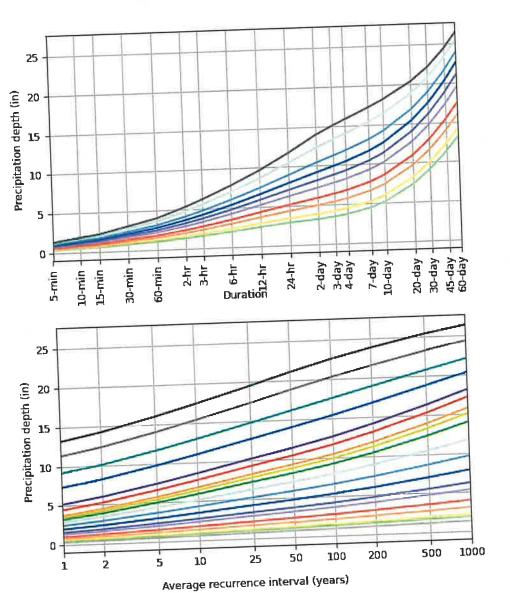
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

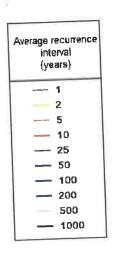
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

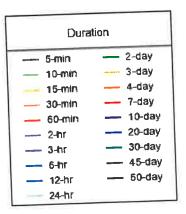
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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 41.3226°, Longitude: -72.2093°







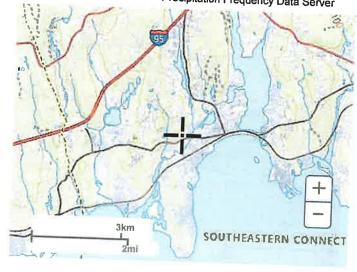
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US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC, Questions@noaa.gov

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NOAA Atlas 14, Volume 10, Version 3 Location name: Niantic, Connecticut, USA* Latitude: 41.3226°, Longitude: -72.2093° Elevation: 32 ft** source: ESRI Maps source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

Durat	ion	based point precipitation frequency estimates with 90% confidence intervals (in inches/						oc/hou		
	1	2	5			nce interval	(years)		till men	es/IIOUr
5-mi	in 4.03 (3.11-5.1	4.82	6.13	7.21	25 8,70	50	100	200	500	1000
10-m	in 2.86	3.42	(4.72-7.81) 4.34	(5.51-9.24)	(6.46-11.5)	9.82 (7.14-13.2)	11.0 (7.80-15.3)	12.3 (8.29-17.4	14.3	15.9
15-mi	(2.20-3.6	3) (2.63-4.35) 2.68	(3.34-5.54)	5.11 (3.90-6.54)	6.16 (4.57-8.18)	6.95 (5.06-9.38)	7.79 (5.52-10.8)	8.74	10.1	(10.1-23
	(1.73-2.8	5) (2.07-3.41)	3.41 (2.62-4.34)	4.01 (3.06-5.14)	4.84 (3.59-6.42)	5.46	6.11	6.86	(6.56-14.7) 7.95	(7.15-16
30-mi	n 1.58 (1.22-2.01	1.89 (1.46-2.41)	2.40 (1.84-3.06)	2.82 (2.16-3.62)	3.41	(3.97-7.36)	(4.33-8.50) 4.30	(4.60-9.66)	(5.14-11.5)	8.86 (5.60-13
60-mii	n 1.02 (0.787-1.3	1.22 (0.941-1.55)	1.55	1.82	(2.53-4.52) 2.20	(2.80-5.18) 2.48	(3.05-5.98)	4.83 (3.24-6.80)	5.59 (3.62-8.09)	6.22 (3.94-9.1
2-hr	0.668 (0.520-0.84	0.800	1.02	1.20	(1.63-2.91)	(1.80-3.34)	2.78 (1.97-3.86)	3.11 (2.09-4.38)	3.60 (2.33-5.21)	4.01
3-hr	0.516	0.619	(0.788-1.29) 0.785	(0.921-1.52)	(1.08-1.90)	1.63 (1.19-2.18)	1.82 (1.30-2.52)	2.05 (1.38-2.86)	2.39	2.67
6-hr	0.329	7) (0.483-0.776) 0.393	(0.611-0.989)	0.924 (0.715-1.17)	1.11 (0.837-1.46)	1.26 (0.926-1.68)	1.41 (1.01-1.94)	1.59	(1.55-3.42) 1.85	(1.70-3.88 2.07
23,1100	0.260-0.409	(0.310-0.490)	0.499 (0.392-0.623)	0.586 0.458-0.735)	0.707	0.797	0.892	(1.07-2.20) 1.00	1.17	(1.32-2.99
12-hr	(0.161-0.250	0.242 (0.192-0.299) 0.143	0.306 (0.243-0.379) ((0.360	0.433	0.488	(0.645-1.22) 0.547	(0.684-1.38)	(0.767-1.65)	1.31 (0.838-1.88
24-hr	0.119 (0.096-0.146)	0.143 (0.115-0.175)	0.182	0.215	0.260	0.293	0.398-0.738)	(0.421-0.838)	0.715 (0.471-1.00)	0.799 (0.514-1.14
2-day	0.066	0.143 (0.115-0.175) (0.080 (0.065-0.098) (0.065-0.098)	0.104	0.123	0.150	.221-0.381) ((0.241-0.441)	0.371 (0.255-0.501)	0.434 (0.287-0.601)	0.487
3-day	0.049	0.000	- L	0.100) [(0	. 110-0.1901 1/0	120 0 2101 10		V.Z 17	0.256	0 204
l-day	0.038	0.010	7 130	0, 1-0, 100) (0.	.084-0.136) ((0	093 0 156V I/O		0.150	0.184	0.200
	0.026	0.00	111.7	10.000) (0.	007-0.10711/61	074 0 1221 Va		0.123	0.145	0.404
'-day	(0.021-0.031)	(0.025-0.037)	0.039 .032-0.047) (0.0	0.046	0.055	0.062	0.069	0.085-0.163) ((0.097-0.197) (0	.107-0.226)
0-day	(0.017-0.025)	0.031 (0.025-0.037) (0. 0.024 (0.020-0.029) (0.	0.030	0.035	0.042	0.047	0.052	.054-0.102) (0	0.091	0.102 066-0.139)
- 11	0.045	0.04	The second second second	20 0.042) (0.0	/33-U.052) I/n n	36 0 DEDULA		V.U36	0.068	0.075
- 1	0.012	0.040	The second of th	10 0.02/) (0.0	21-0.0321110 n	22.0 0361 /0 6		0.034	0.039	0.040
	0.010	0.011	-	0.02 () ((0.0	10-0.024) I/O O	17 0 0271 /0 0	established decreased from the	0.026	0.028	0.000
	0.000		The second second	. 5.010) [[0.0	12-0.019) (0.04	3 0 0041 100 0		0.019	0.024	0.000
uay (0.007-0.010) (0 frequency (PF arenthesis are I	0.009 0.008-0.011) (0.0) estimates in this	09-0 012) (0 01	0.012	0.013 0	.014	0.025) (0.0	114-0.025) (0.0	014-0.028) (0.0	14-0.029)

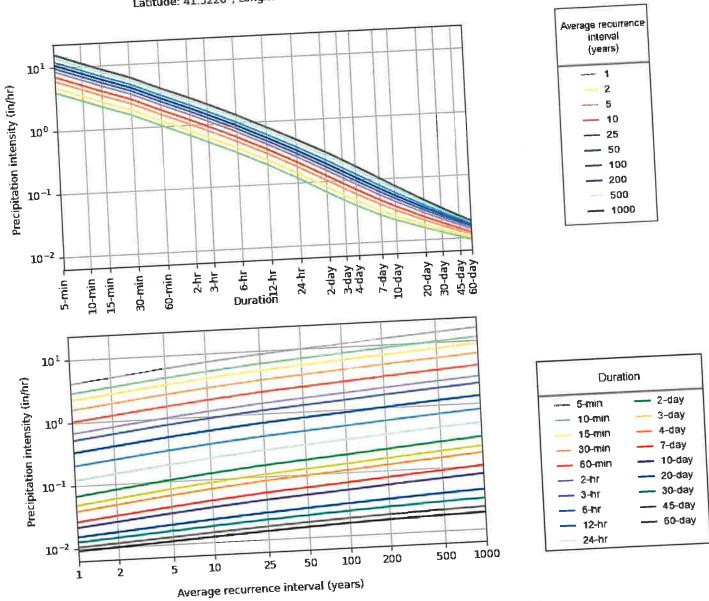
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 41.3226°, Longitude: -72.2093°



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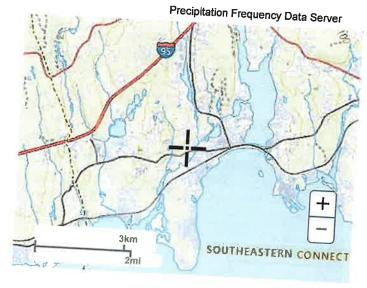
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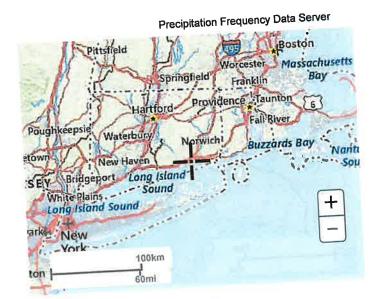
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Large scale aerial



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National Water Center
1325 East West Highway
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